

Do we need to consider dispersive troposphere delays for current and next generation space-geodetic instruments?

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Refractivity

Current model used for micro-wave techniques in space geodesy

$$N = \overbrace{N_0(P, T, RH)} + \underbrace{N'(P, T, RH, f) + i \cdot N''(P, T, RH, f)}$$

Frequency dependent complex contribution which is neglected for micro-wave techniques.

Real part → delay

Imaginary part → damping

Question: *Can we really neglect the dispersive part for current and upcoming space geodetic techniques ?*

Liebe93 Model (dispersive terms only)

$$N(f) = N_D(f) + N_V(f) \quad (\text{Note: these are all complex functions!})$$

Dry-Air Module

$$N_D(f) = N_n(f) + \sum_k S_k(f) F_k(f)$$

$N_n(f)$ non-resonant term of the O_2 spectrum

$S_k(f)$ line strength of the k-th O_2 line

$F_k(f)$ Van Vleck-Weisskopf function

44 oxygen lines

Water Vapor Module

$$N_V(f) = N_c(f) + \sum_l S_l(f) F_l(f)$$

$N_c(f)$ H_2O continuum spectrum

$S_l(f)$ line strength of the l-th H_2O line

$F_l(f)$ Van Vleck-Weisskopf function

34 H_2O lines

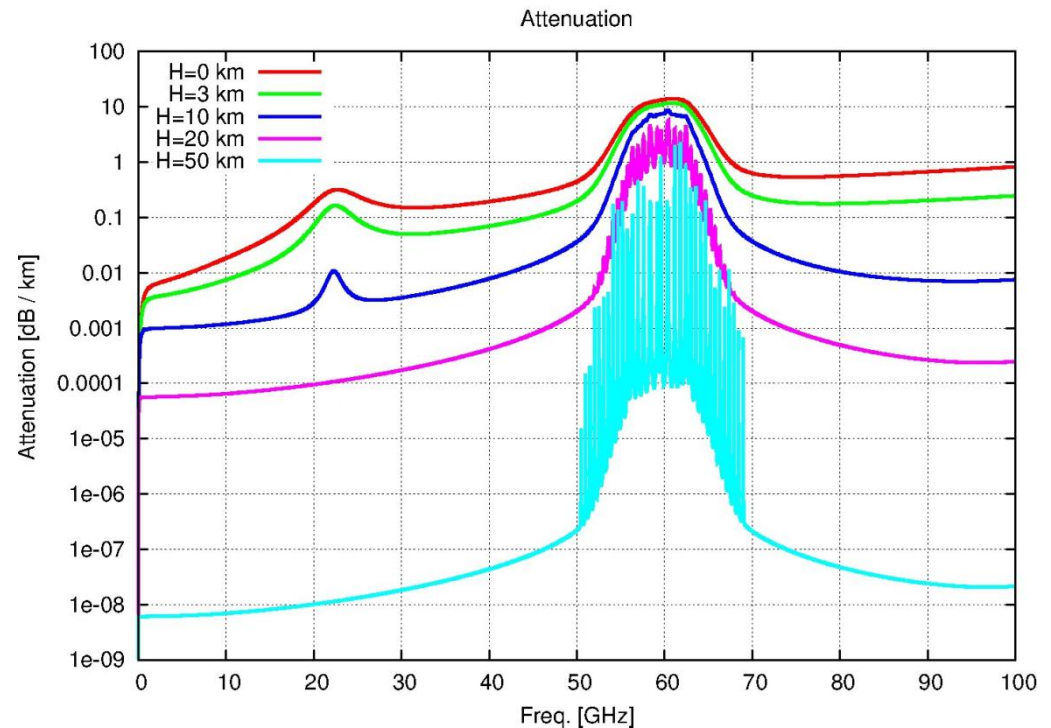
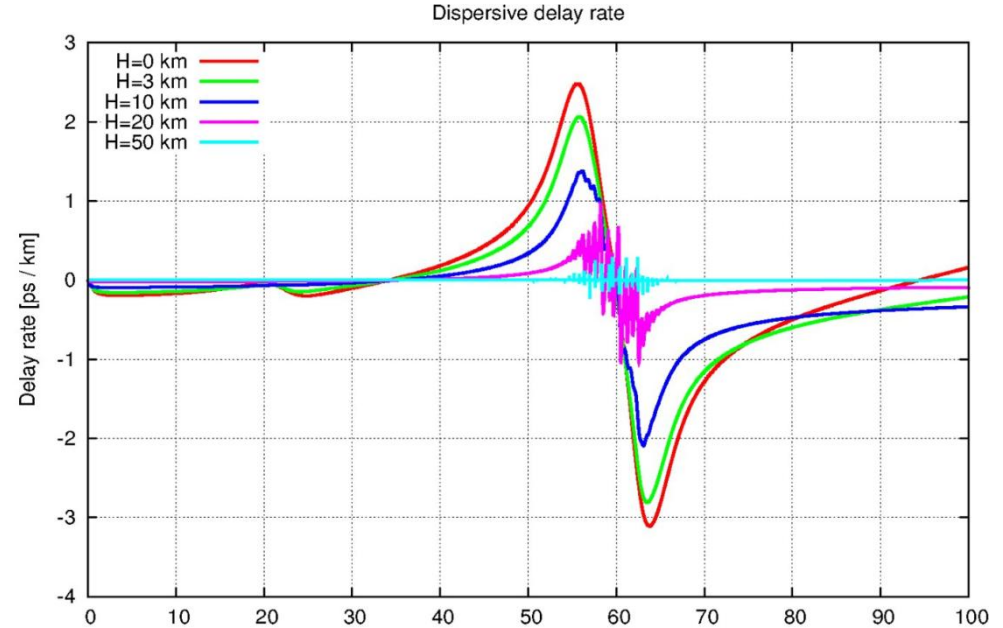
Liebe93 model has been adopted in the ITU-R recommendation P.676-8:

“ ... valid for the frequency range between 1 – 1,000 GHz ... ”

Simulations:

- P and T from US standard atmosphere
- RH = 50 for H < 13 km
- RH = 0 for H > 13 km

- Space geodetic microwave techniques are not operating close to the O₂ lines
- However, there are significant slopes of the real part (delay) which need to be studied for dual-frequency techniques!

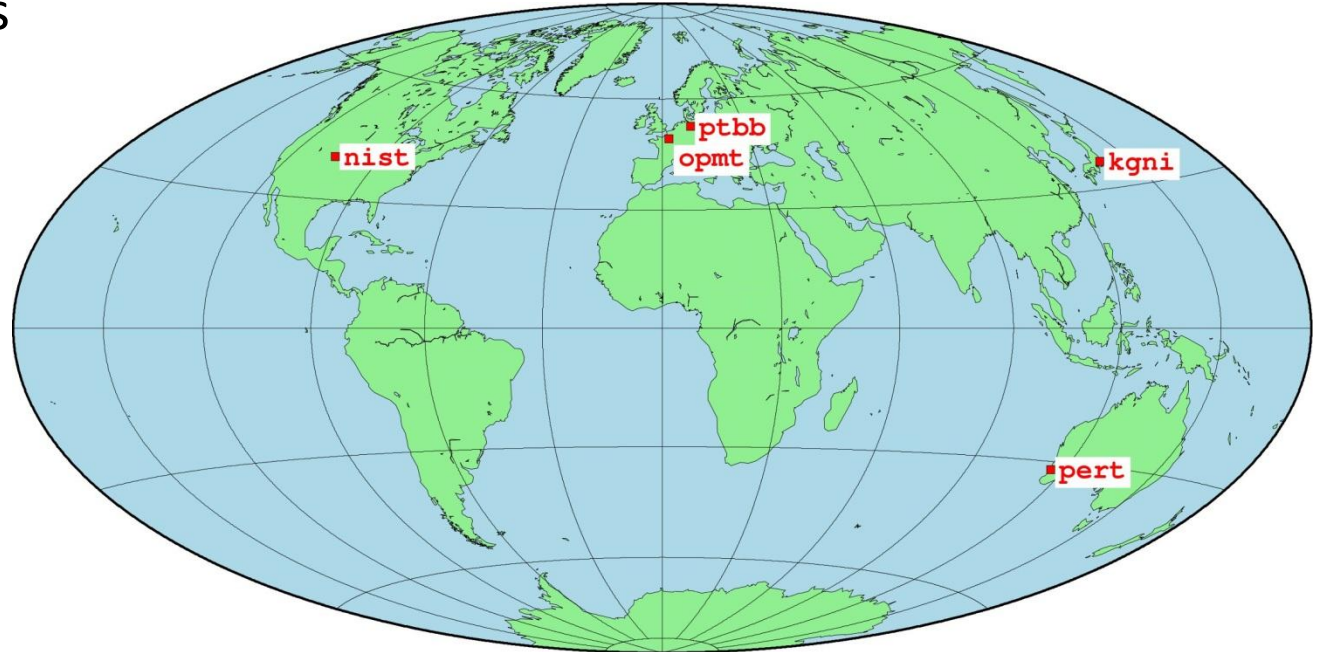


KARAT- λ

- Modified version of our ray-tracer KARAT (Hobiger et al., JGR, 2008)
- Carries out ray-tracing in long-double precision
- Computes complex refractivity values for a given frequency based on data from a numerical weather model (P, T, RH)
- Very time consuming calculations
- Requires large CPU memory (> 8 GB)
- Benefit: allows to derive signal attenuation by integrating over the imaginary part of the refractivity index → tool for radio-communication (link budget, signal fading, etc...)

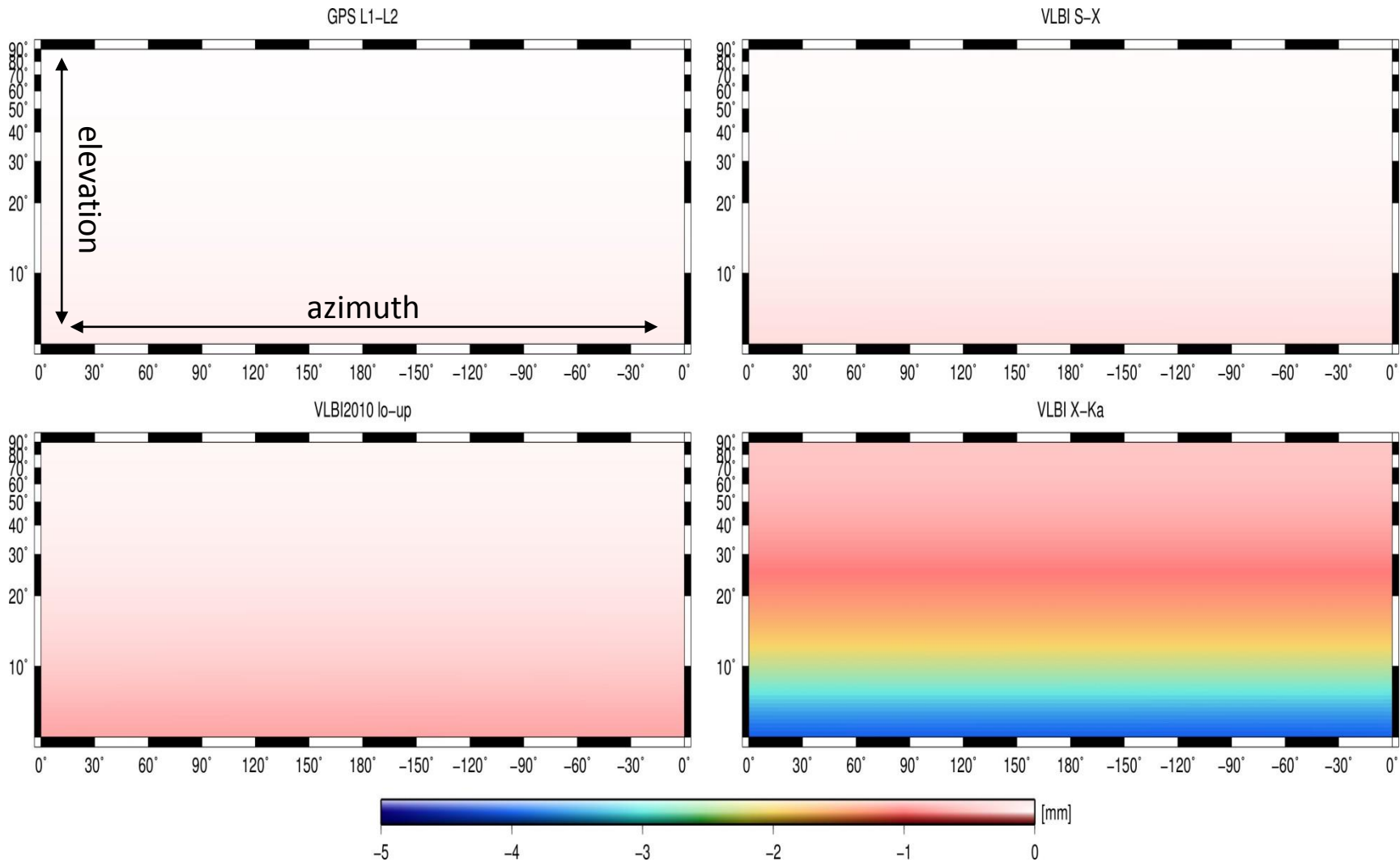
Simulations

- 5 Stations

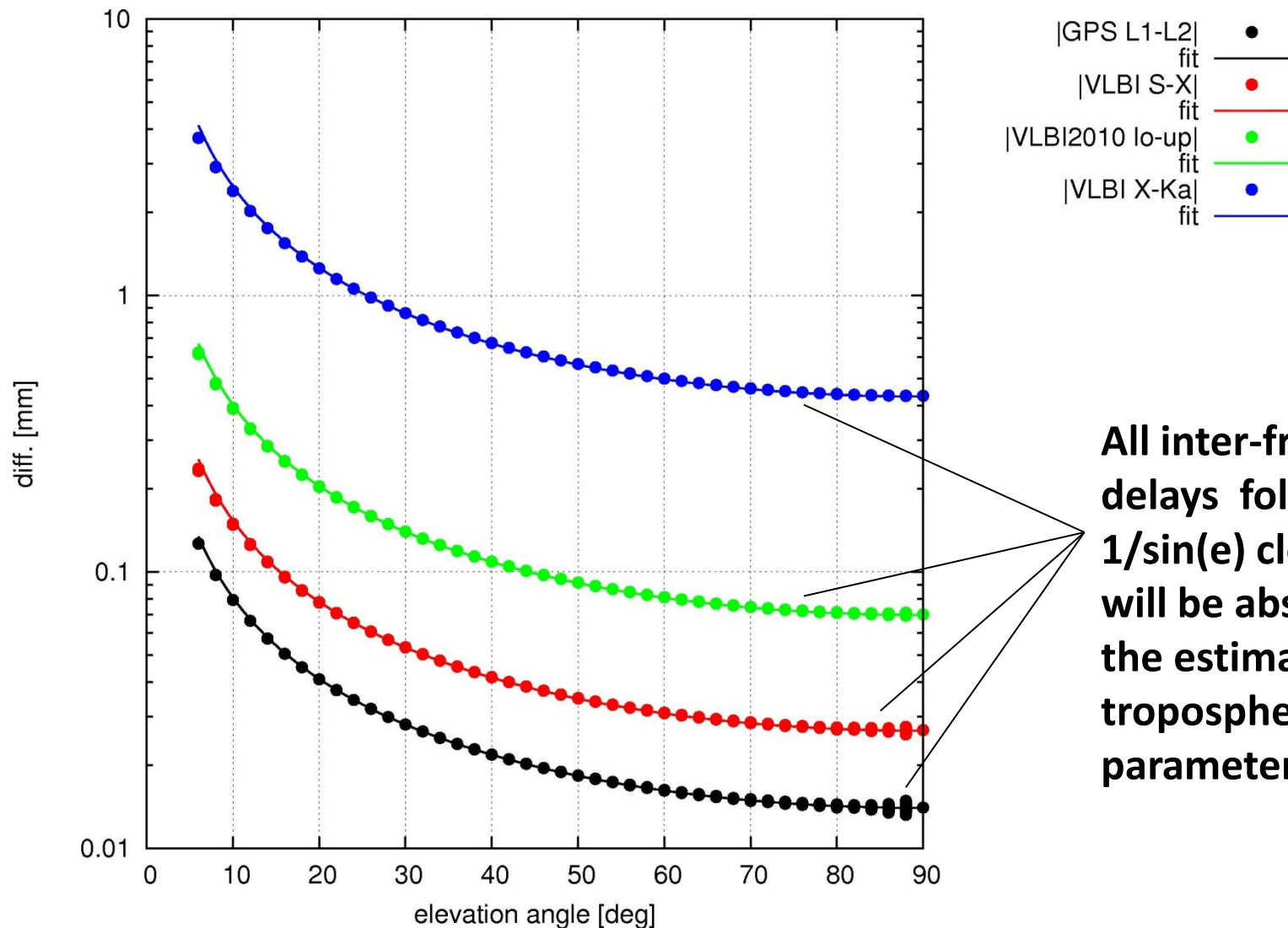


- ECMWF data (0.2 x 0.2 deg) between Aug. 1st and Aug. 7th, 2011
- Every day at 0 UT, delays in all azimuth directions and for elevation angles between 6 and 90 degree
- Space geodetic techniques considered
 - GPS-L1, GPS-L2
 - VLBI-S (2.3 GHz), VLBI-X (8.4 GHz)
 - VLBI2010-lowest band (2.5 GHz), VLBI2010-highest band (11.7 GHz)
 - VLBI-X (8.4 GHz), VLBI-Ka (32 GHz)

Results (Koganei, Japan, Aug. 1st, 2011, 0 UT)



Elevation dependency (Koganei, Aug. 1st, 2011, 0 UT)



All inter-frequency delays follow $1/\sin(e)$ closely → will be absorbed by the estimated troposphere parameters !

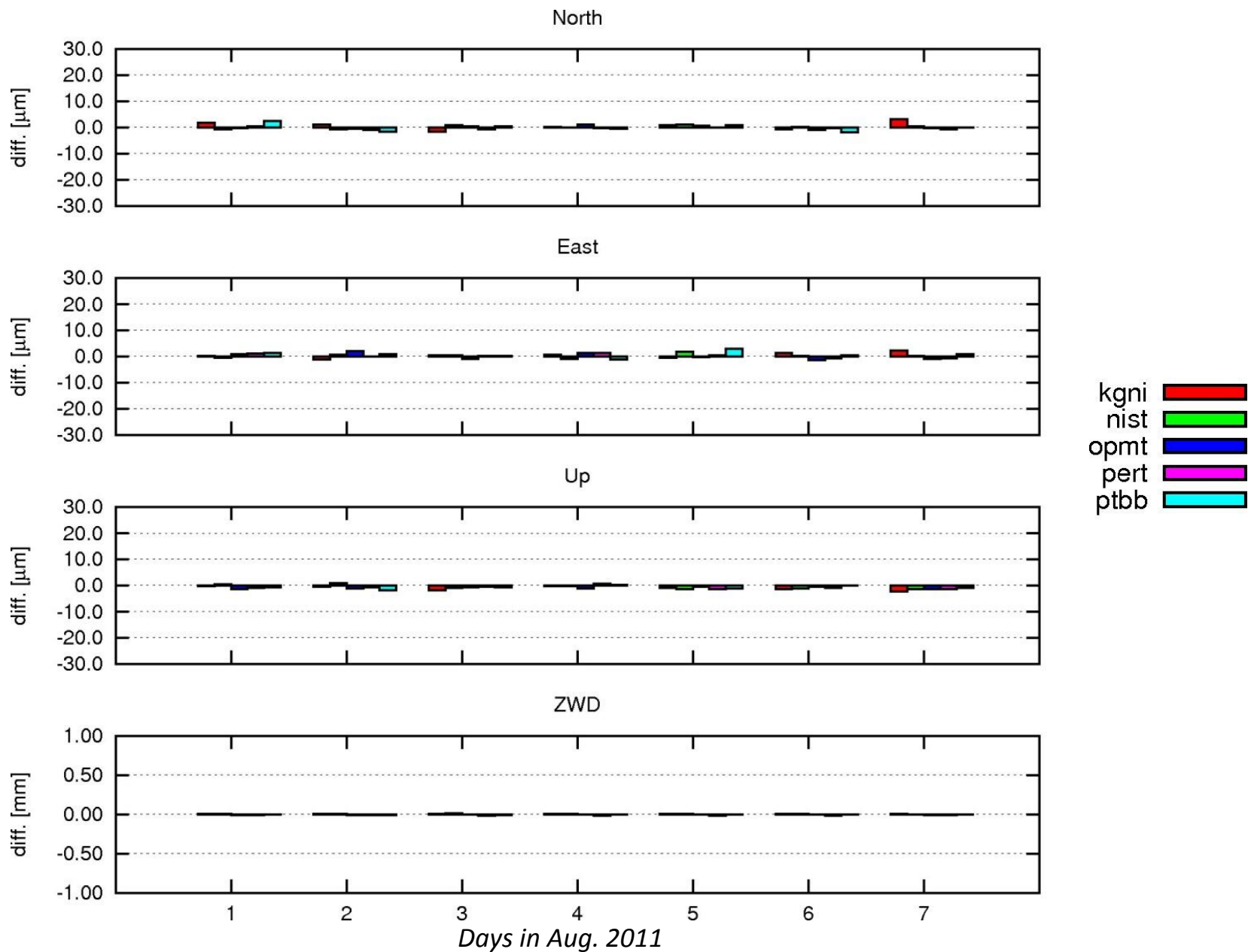
Effect on geodetic parameter estimation

- Assume 4 unknowns position (N,E,U) + ZWD
- Utilize ray-traced dispersive troposphere total delays and form the ionosphere-free linear combination

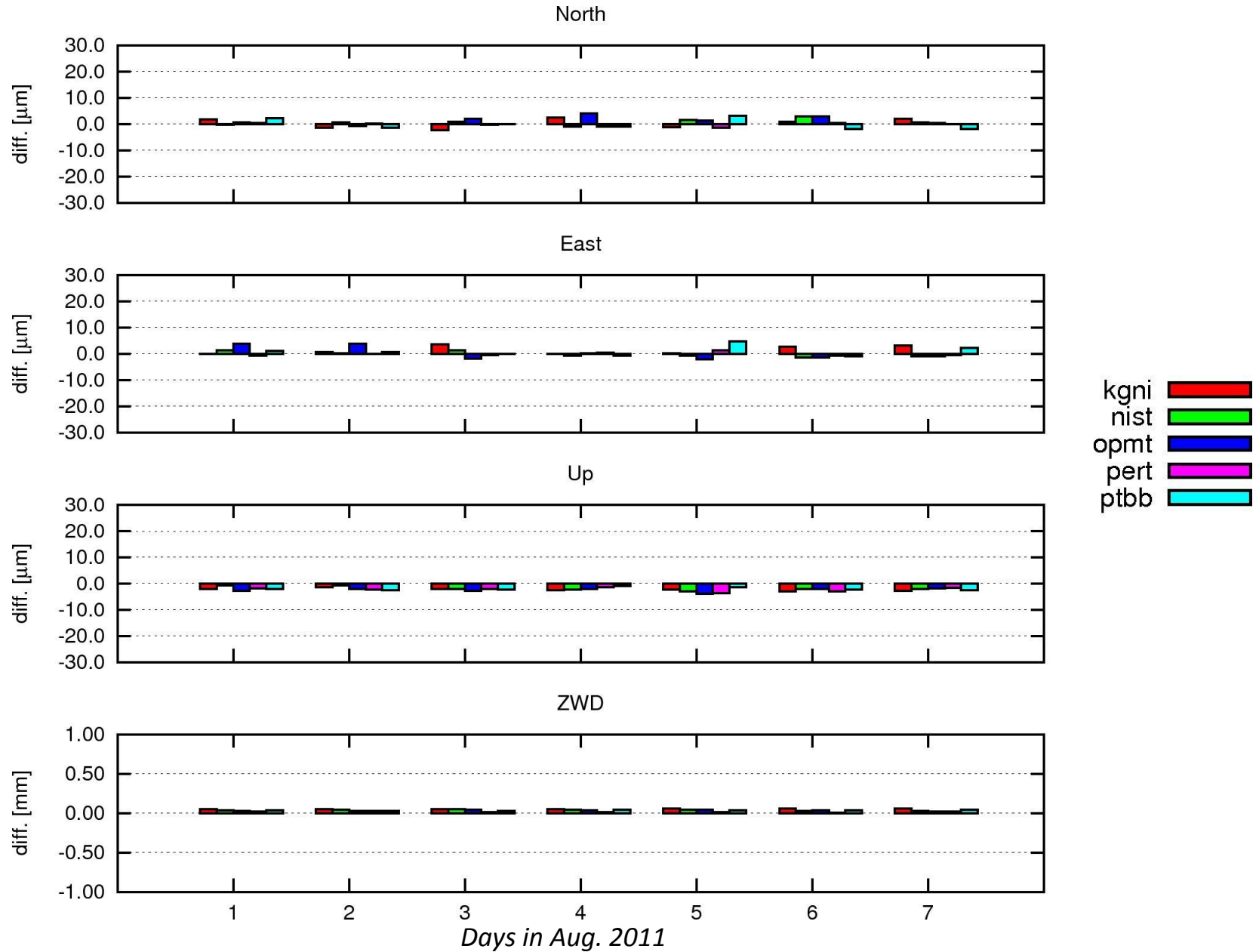
$$\tau = \frac{f_1^2}{f_1^2 - f_2^2} \tau_1 - \frac{f_2^2}{f_1^2 - f_2^2} \tau_2$$

- Mapping function: GMF
- ZHD: Saastamoinen model, based on T and P at the station as obtained from numerical weather model
- Computing the differences w.r.t. the GPS L1/L2 position and ZWD estimates

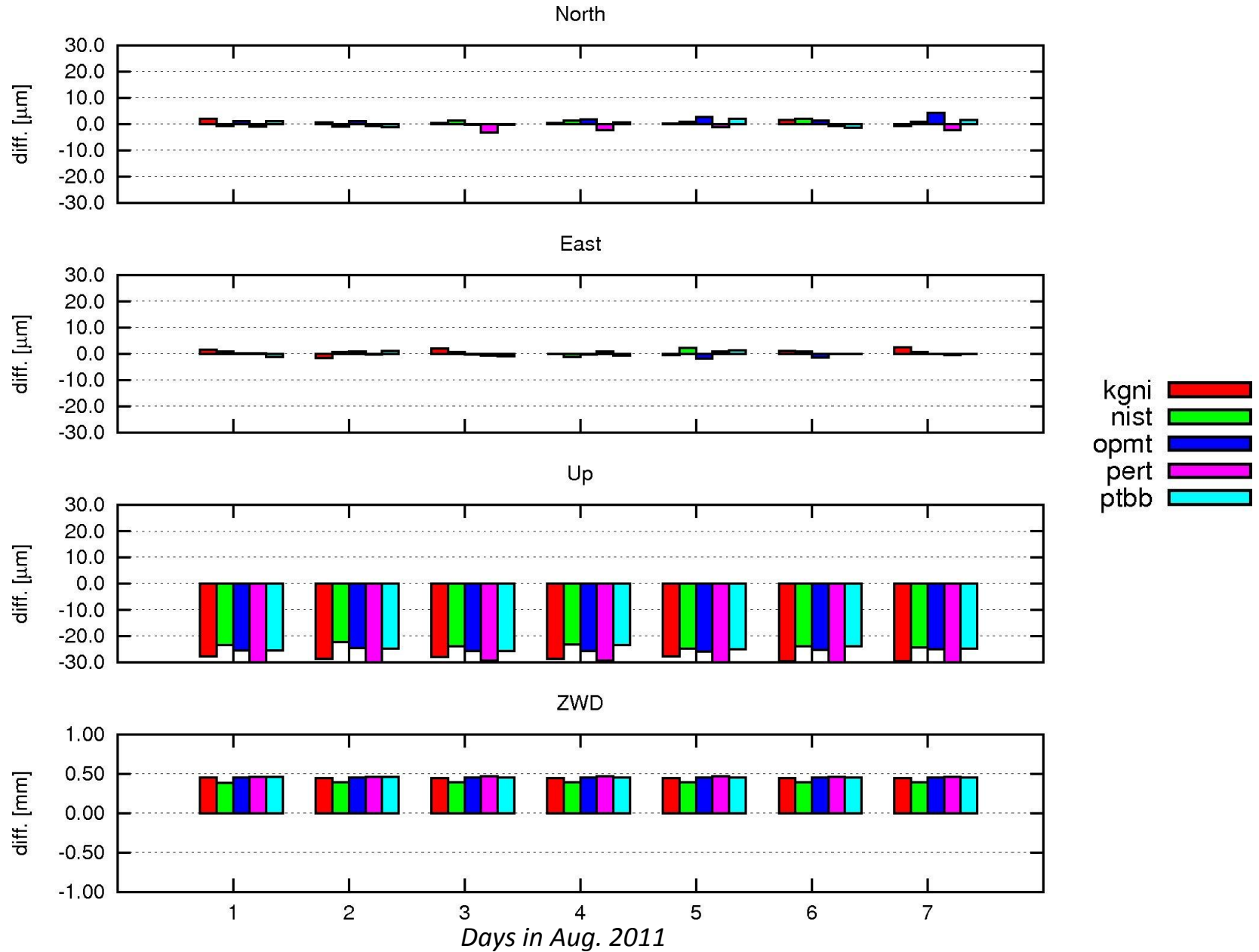
VLBI S/X w.r.t. GPS L1/L2



VLBI2010 w.r.t. GPS L1/L2



VLBI X/Ka w.r.t. GPS L1/L2



Conclusions

- For current and upcoming space geodetic techniques dispersive troposphere delays
 - reach several mm at very low elevation angles, but are absorbed into the troposphere parameters.
 - have no significant impact on geodetic target parameters
 - bias troposphere parameters by less than 0.1 mm (except X/Ka VLBI)
 - Only VLBI in X/Ka mode should be treated with care when combining troposphere parameters in the (far) future

***Thank you very
much for your
attention.***

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