

# RFI Influence, Survey for Broadband VLBI

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1: NICT/Kashima Space Technology Center, Japan

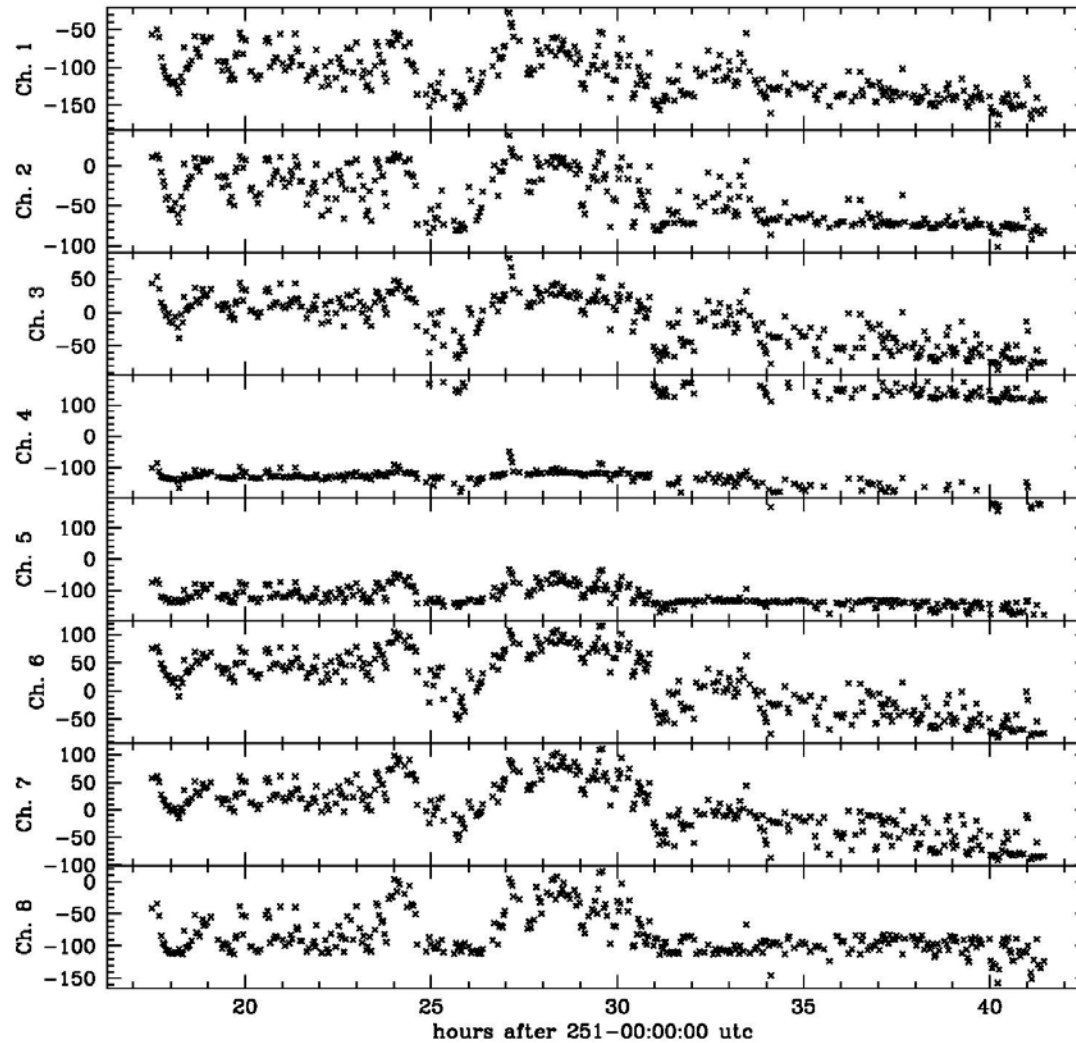
2: MIT/Haystack Observatory, USA

# Contents

- Internal RFI to Phase-cal signal
- RFI Survey for Broadband Observation: Case of NICT(GALA-V)
  - Measurement of RFI represented with  $T_{ant}$
  - Measurement equipment
  - Sources of RFI
  - Measurement of RFI from Broadcasting Satellite.
  - Robustness to RFI: Advantage of RF-Direct sampling
- Experience of Serious RFI to Saturate LNA

# RFI to Phase-cal signal@Kas34

Kashima34 RD1608 X-band pcal phase time series

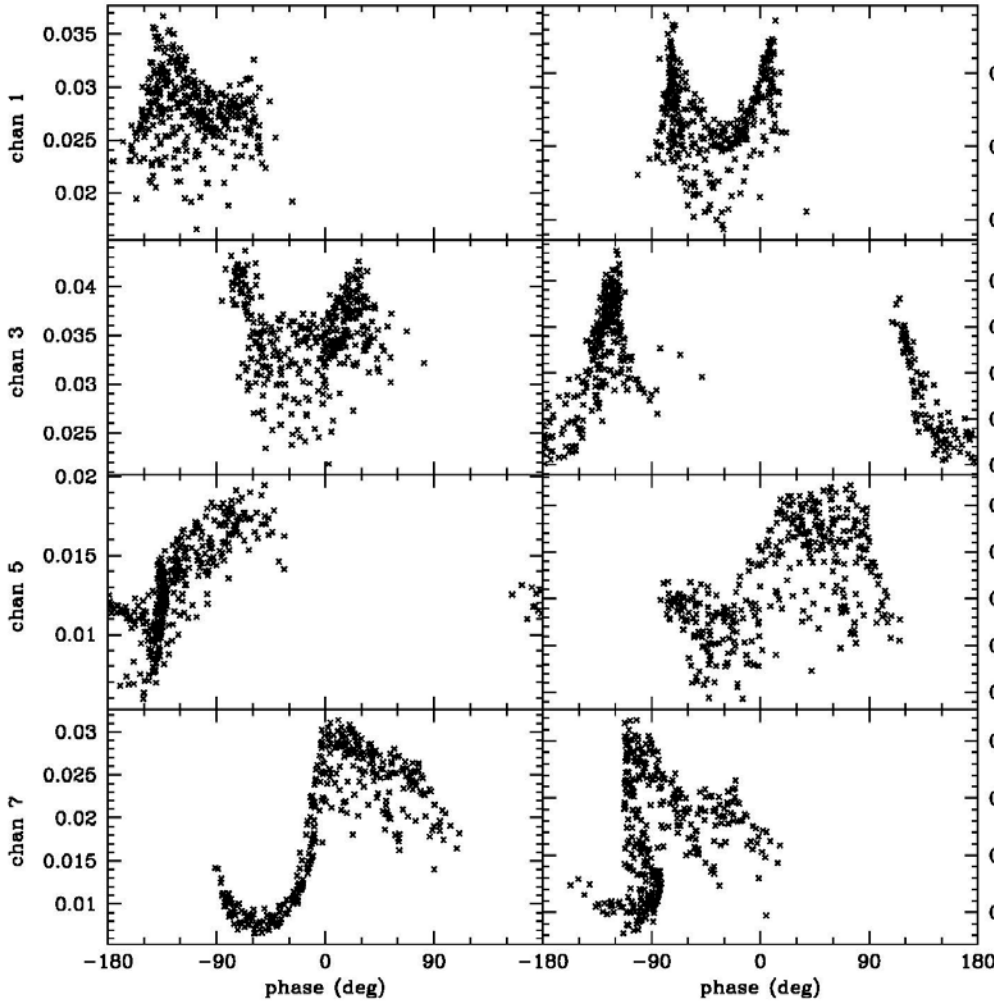


Time vs Phase

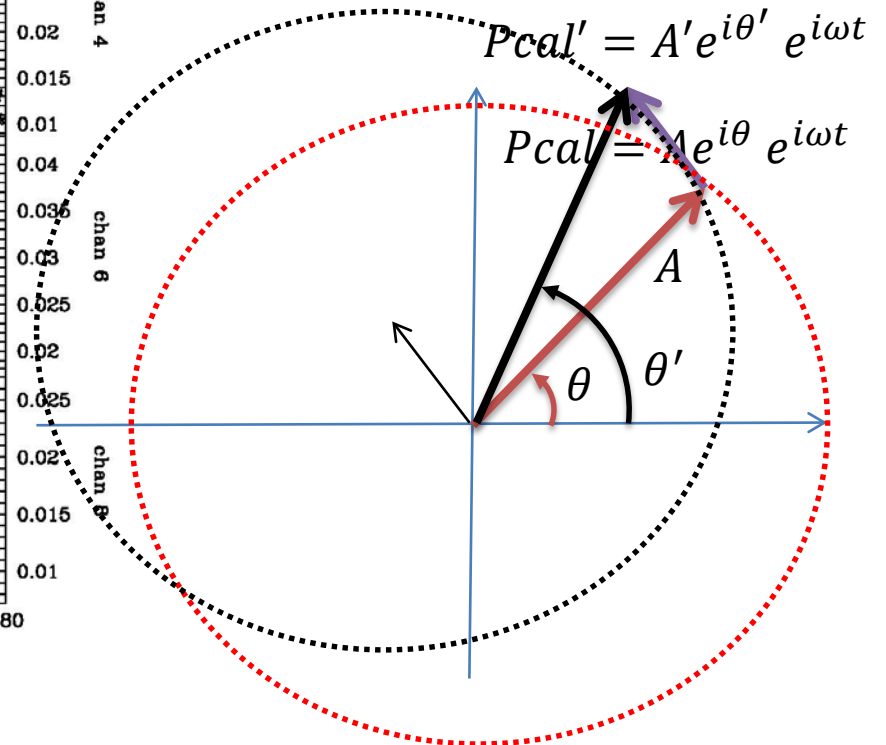
Suggested by  
MIT/C.Brian

# RFI to Phase-cal signal@Kas34

Kashima34 RD1608 X-band pcal amp vs. phase

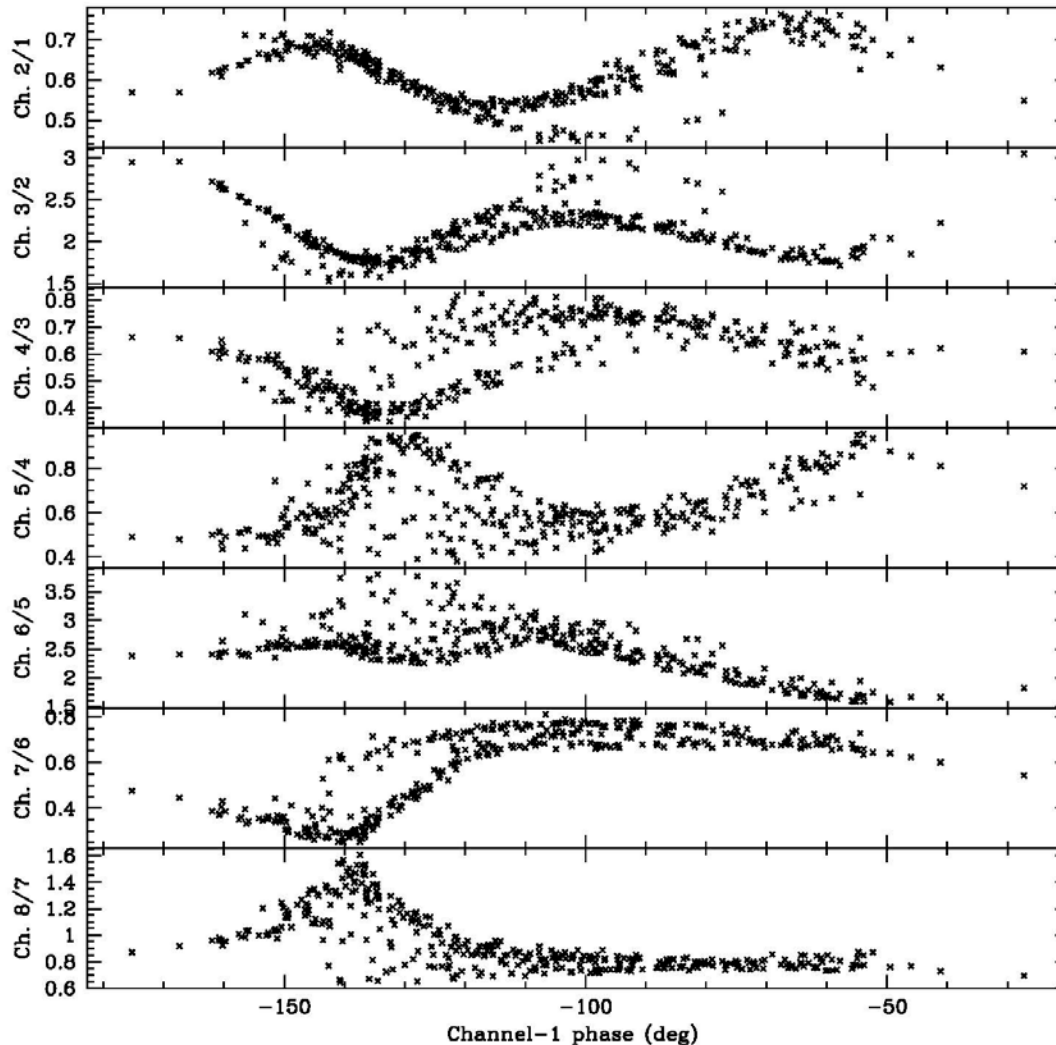


Phase vs Amp  
Suggested by  
MIT/C.Brian

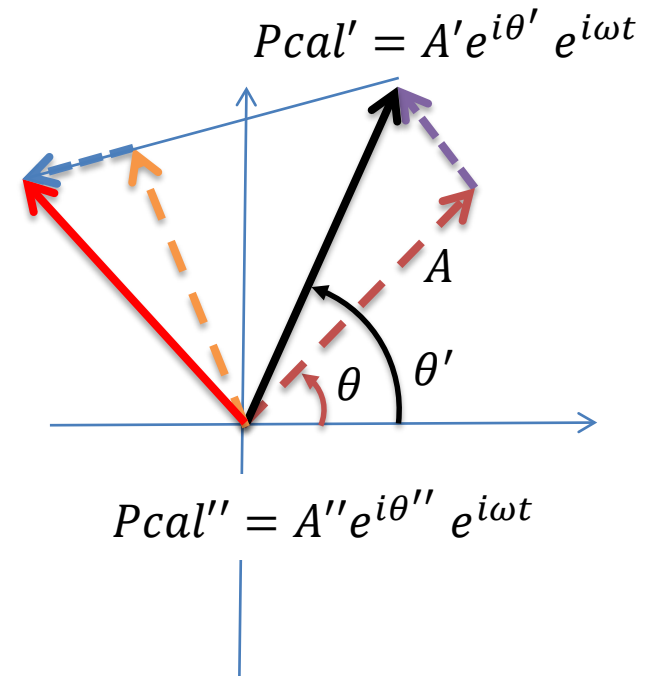


# RFI to Phase-cal signal@Kas34

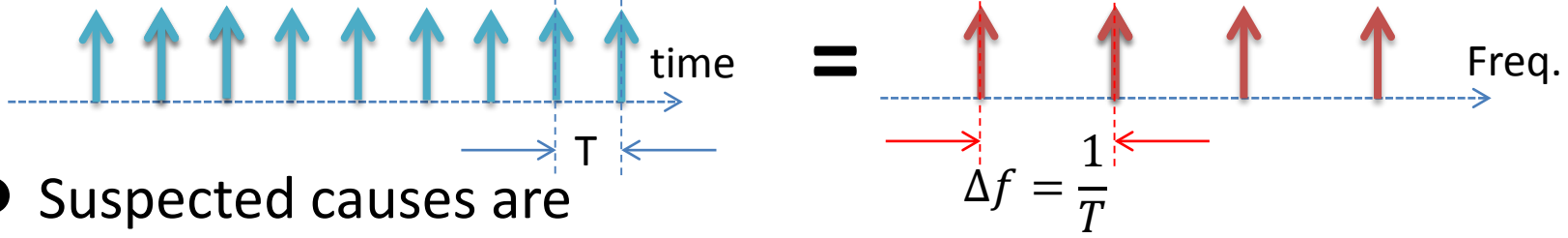
Kashima34 RD1608 X-band channel pcal amp ratio vs. phase



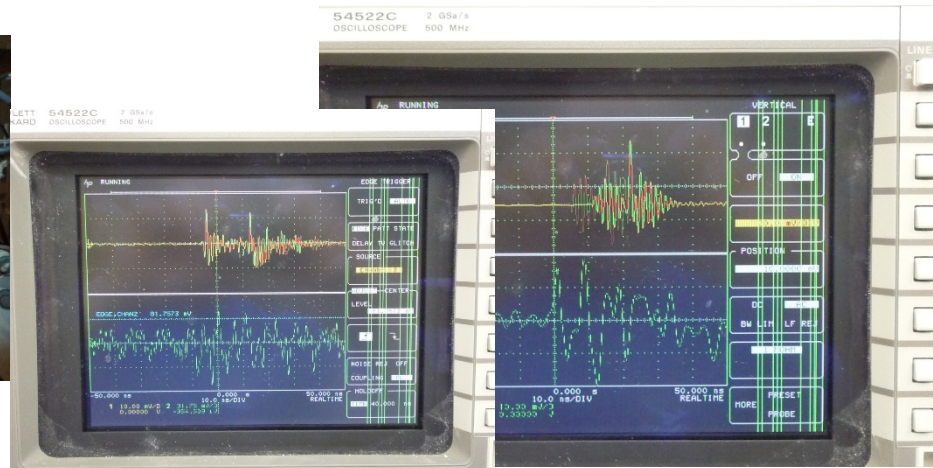
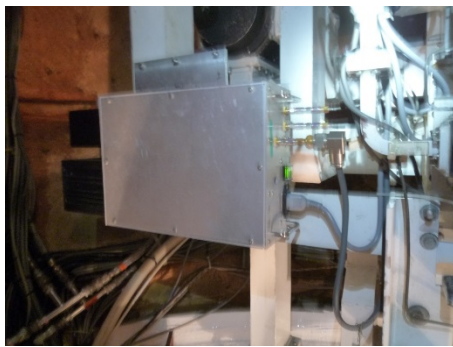
Phase vs Amp Ratio  
Suggested by  
MIT/C.Brian



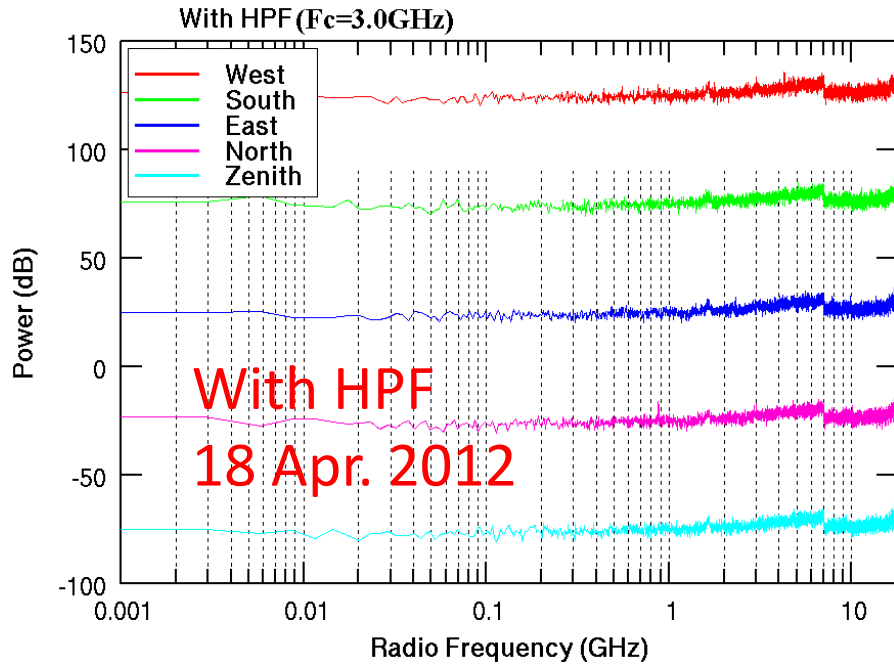
# RFI to Phase-cal signal@Kashima34m



- Suspected causes are
  - A) Re-entry of emission from Pcal antenna unit into the receiver feed.
  - B) Contamination of Pcal signal by distorted signal.
- Investigation:
  - We wrapped Pcal antenna unit by aluminum foil to suppress emission. Though no significant improvement. Thus cause A) seems to be rejected.
  - Pcal pulse signal shape in time domain might resulting cause B), just in case.



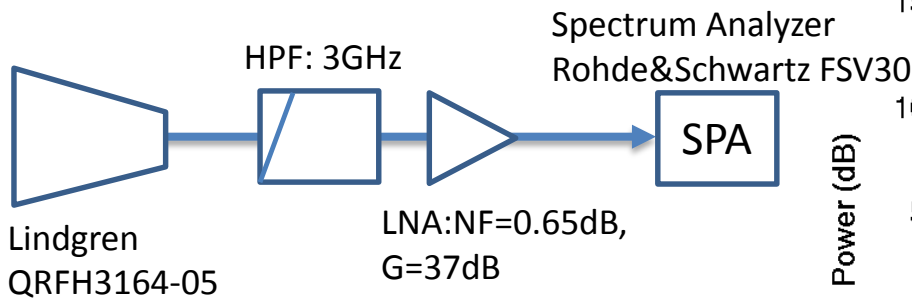
# Lesson from Broadband Observation



EST-Lidgren's Model 3164-05 One-Way Horn

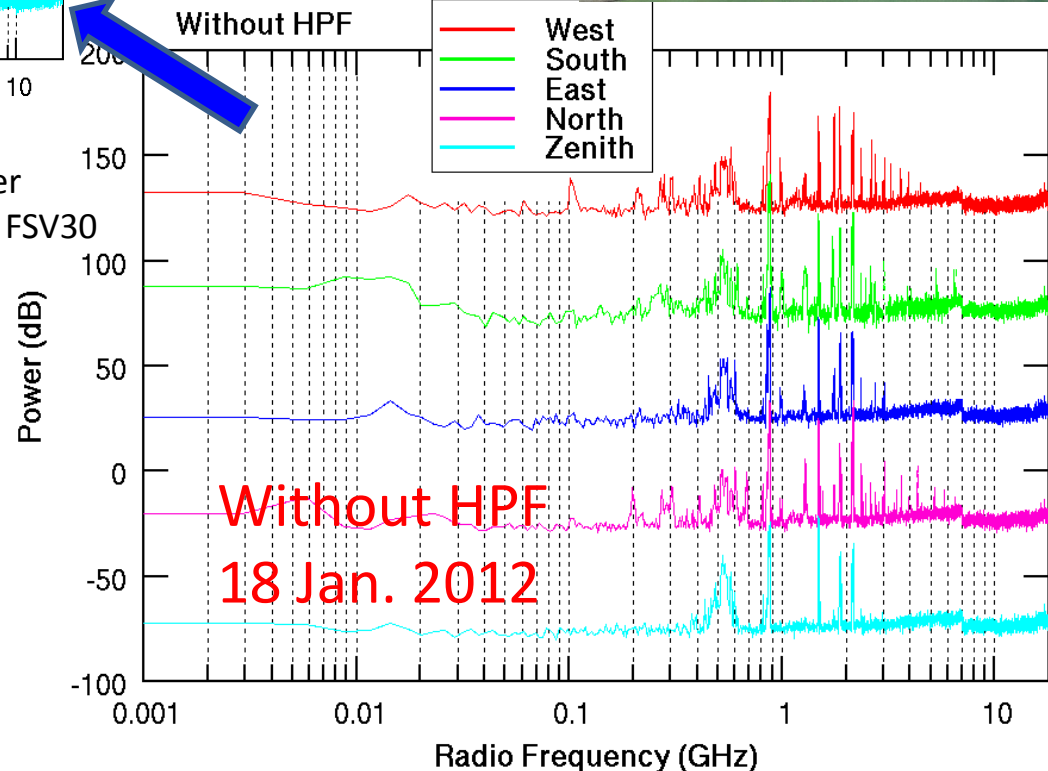


RFI@1.6m MARBLE1  
EST-Lidgren 3164-5  
Broadband Antenna  
RBW=500kHz

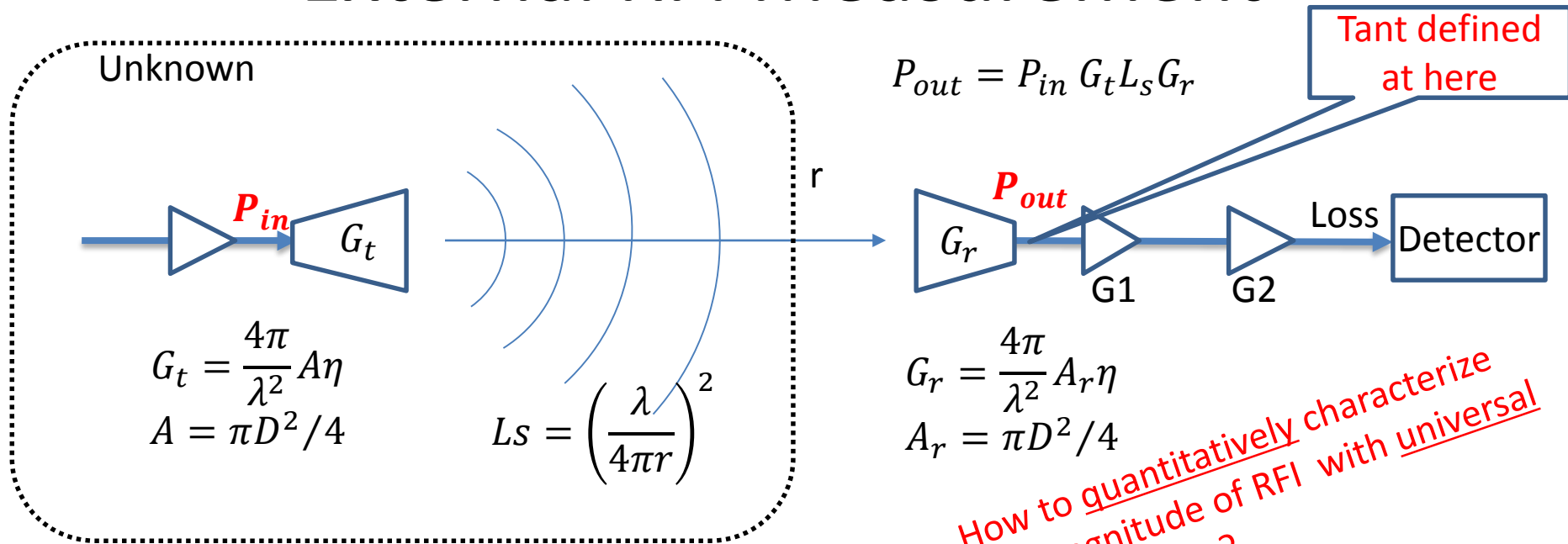


RFI (Mag: 50dB) is eliminated by HPF (3GHz)  
At initial stage of MARBLE 1.6m  
(Broadband antenna)

**High Pass Filtering is Necessary!!**



# External RFI Measurement



## Conditions:

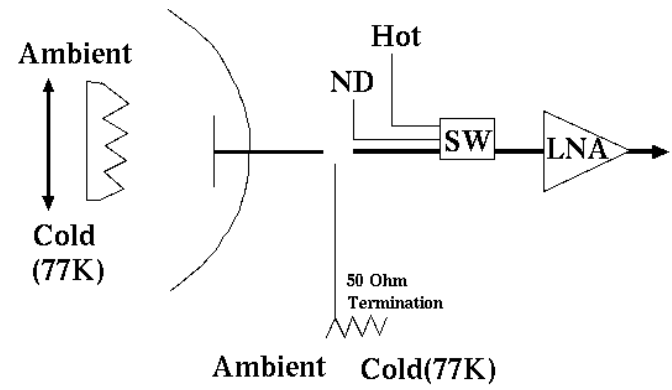
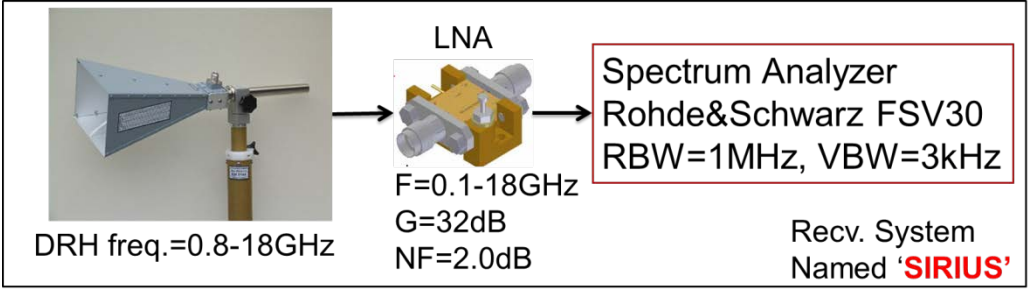
- Receiving power of RFI at Antenna feed depend on  $G_r$
- Receiving power of RFI at Detector depend on  $G_r, G_1, G_2,$  and Loss of the receiver.
- Ratio of RFI power w.r.t. noise level depend on the receiving bandwidth.

## Our Strategy:

- We use RFI input power defined by Antenna temperature after calibration of receiver gain under the condition the receiving system works in linear response region..
- **Advantages:** Free from RBW of measurement, Easy to understand the influence for radio telescopes.
- **Drawback:** Antenna temperature depend on the antenna gain used for measurement.



# Tsky,Trx Measurement by Y-factor



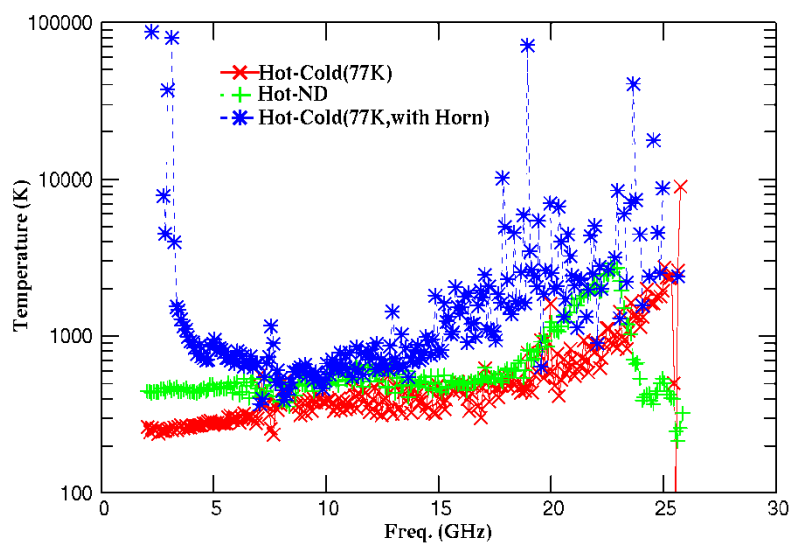
$$Y_1 = \frac{P_{ND}}{P_{Hot}} = \frac{T_{rx} + T_{ND}}{T_{rx} + T_{Hot}}$$

$$Y_2 = \frac{P_{Sky}}{P_{Hot}} = \frac{T_{rx} + T_{Sky}}{T_{rx} + T_{Hot}}$$



$$T_{rx} = \frac{T_{ND} + Y_1 \cdot T_{Hot}}{Y_1 - 1}$$

$$T_{Sky} = Y_2 \cdot (T_{rx} + T_{Hot}) - T_{rx}$$



## Equipment:

- FEED: Schwarzbeck BBHA-9120D (0.8-18.5GHz)
- LNA: B&Z BZP118UD1 (G=32dB, NF=2dB, f=0.1-18GHz)
- Spectrum Analyzer: Rohde&Schwarz FSV30

## Measurement Condition:

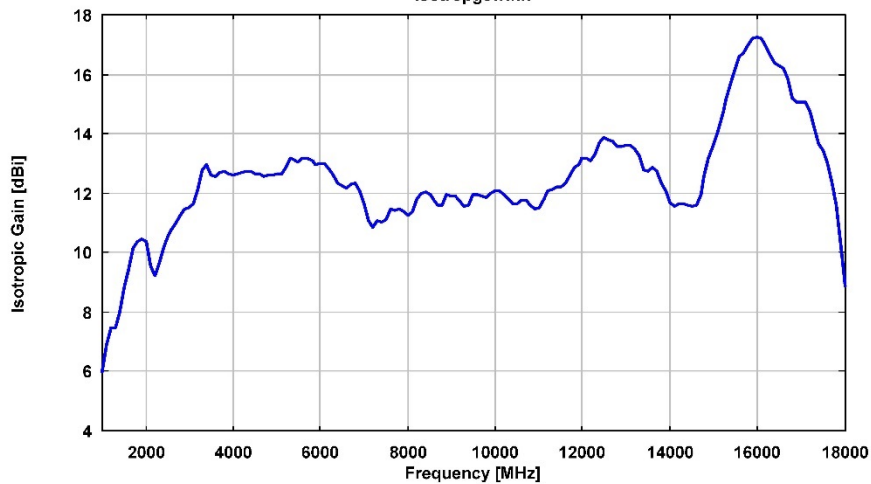
- Polarization-V(all sites), H(NMIJ)
- North/East/South/West Directions

# SchwarzBeck9120D Double Ridged Horn

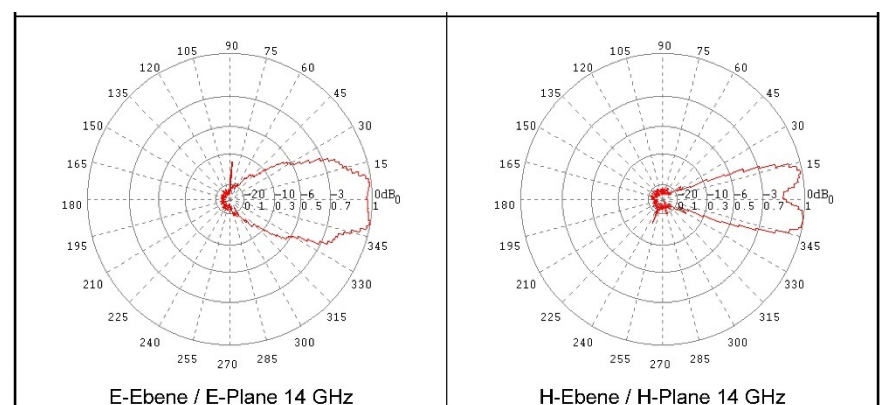
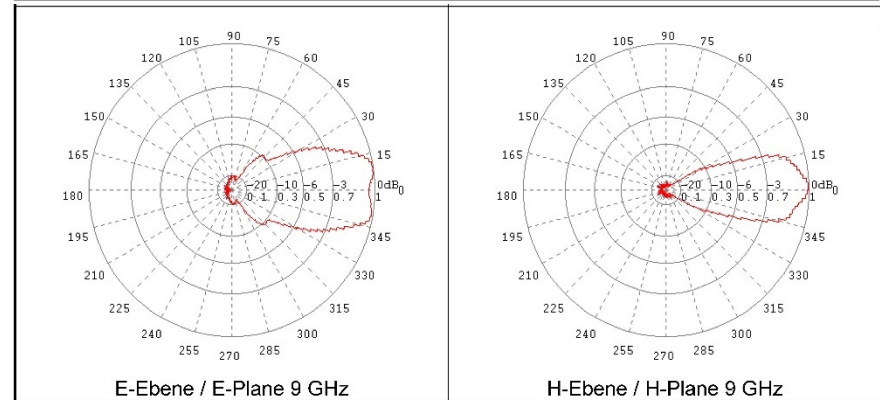
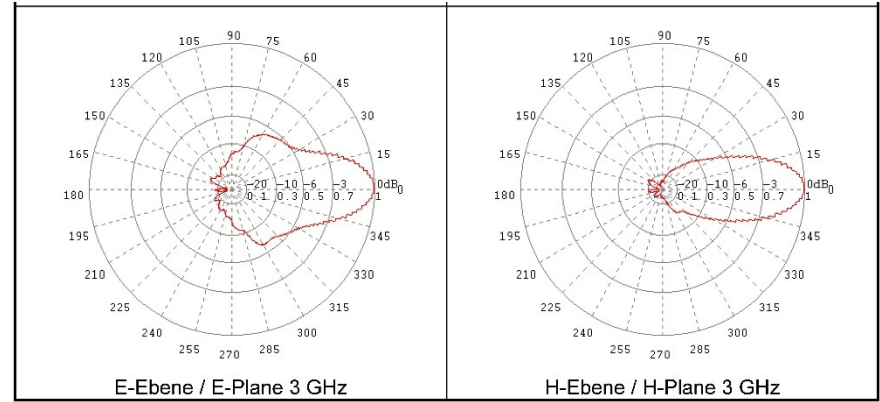
Beam width  $\sim 30$  deg.



Isotropiegewinn



Beam pattern of survey antenna



# Broadband RFI Survey Sites

## NICT-HQ(Koganei)



RF of 2<sup>nd</sup> Building. Communication Antenna for TWSFTT(14GHz), Other emission from experimental system of NICT Labs.

## NMIJ(Tsukuba)



Communication Antenna for TWSFTT(not used).

## NICT (Kashima)

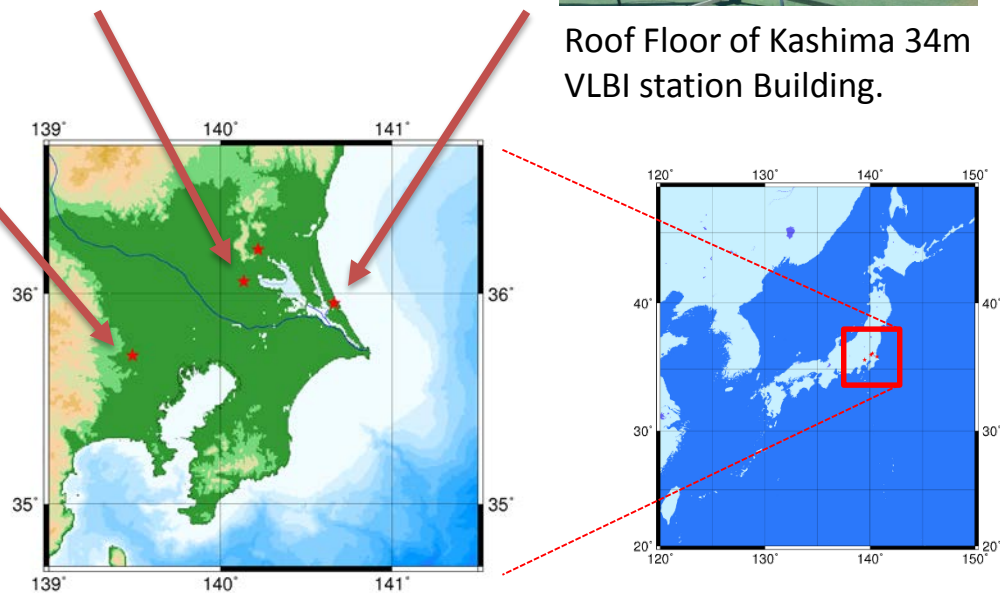


Roof Floor of Kashima 34m VLBI station Building.

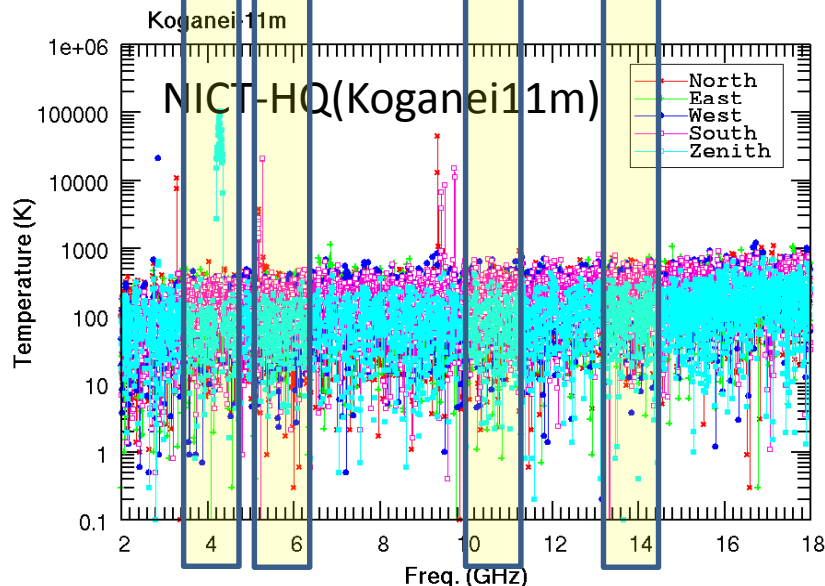
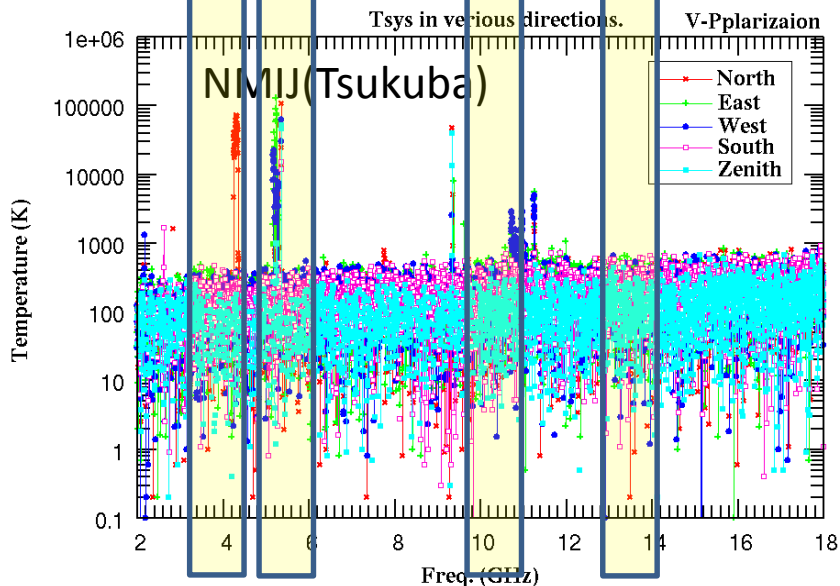
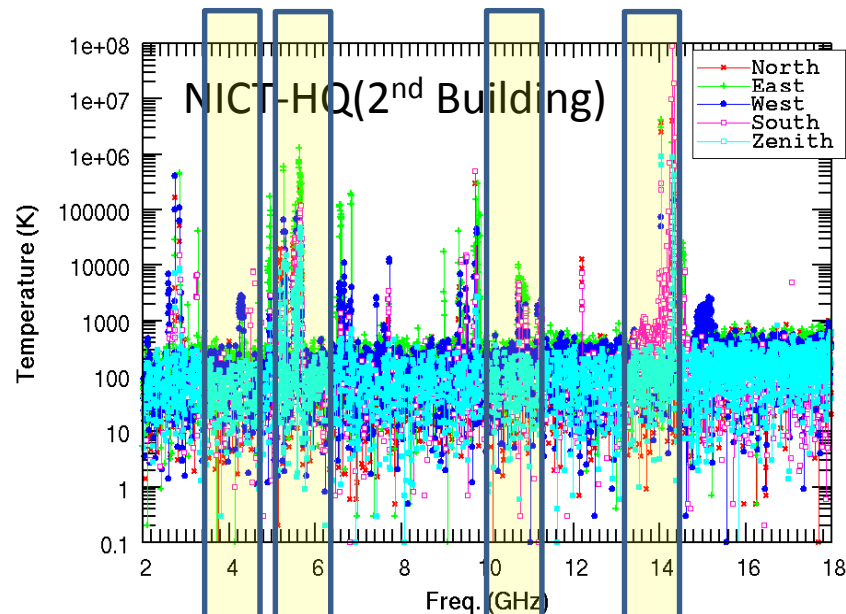
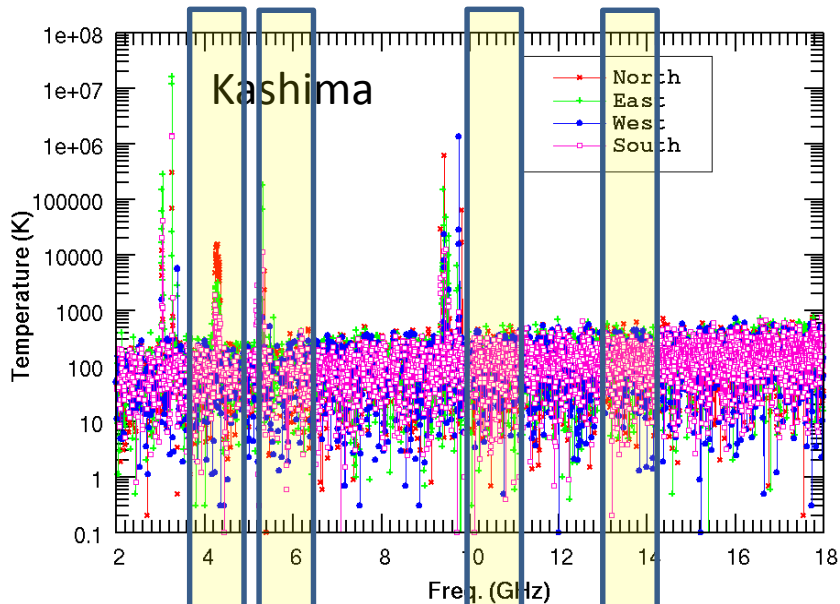
## NICT-HQ(Koganei 11m)



Roof Floor of Koganei 11m VLBI station Building. Relatively quiet. Surrounded by trees.

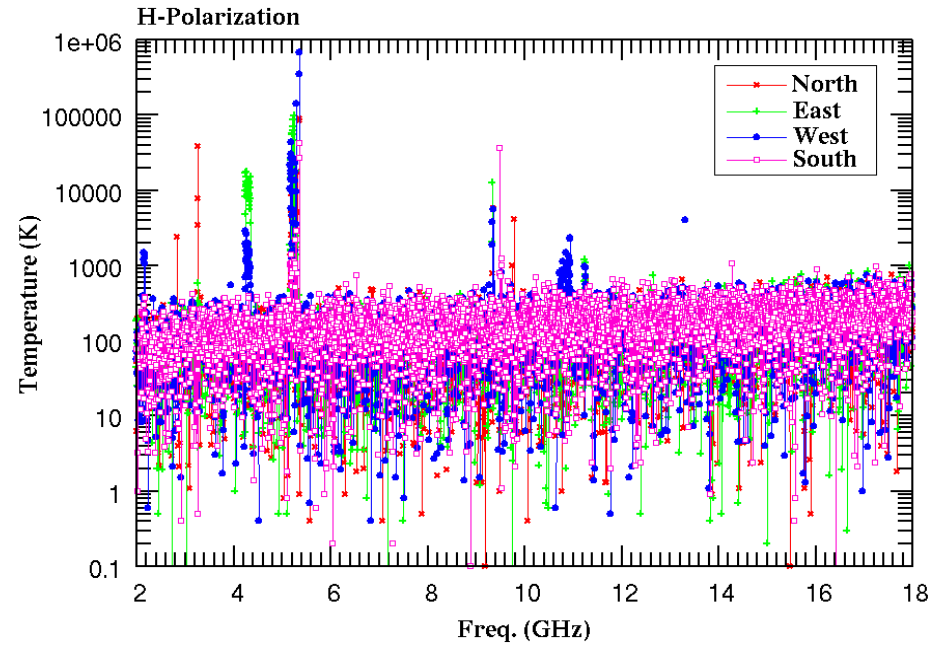
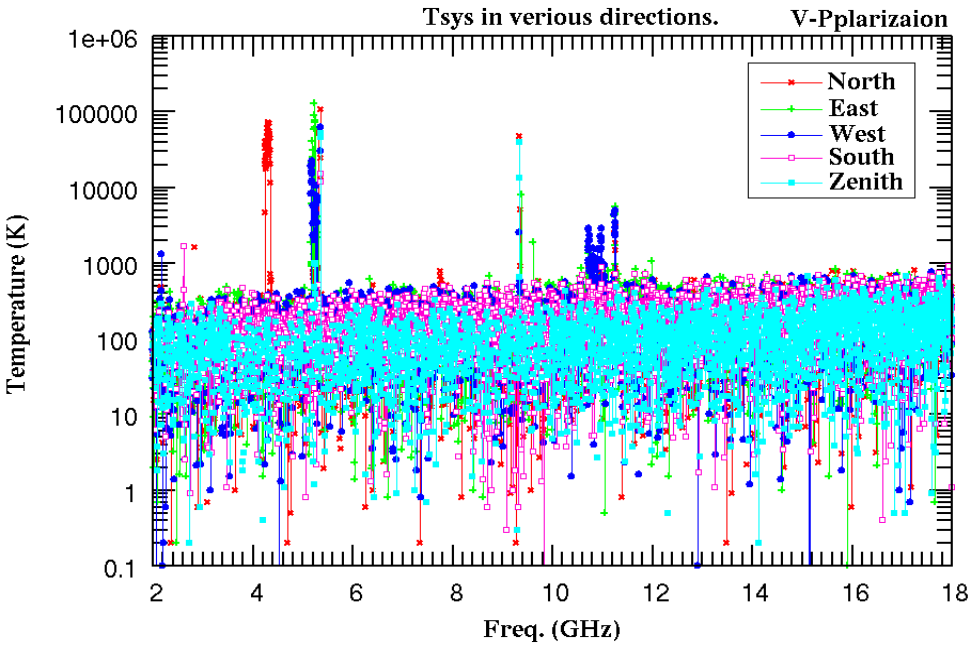


# V-Polarization

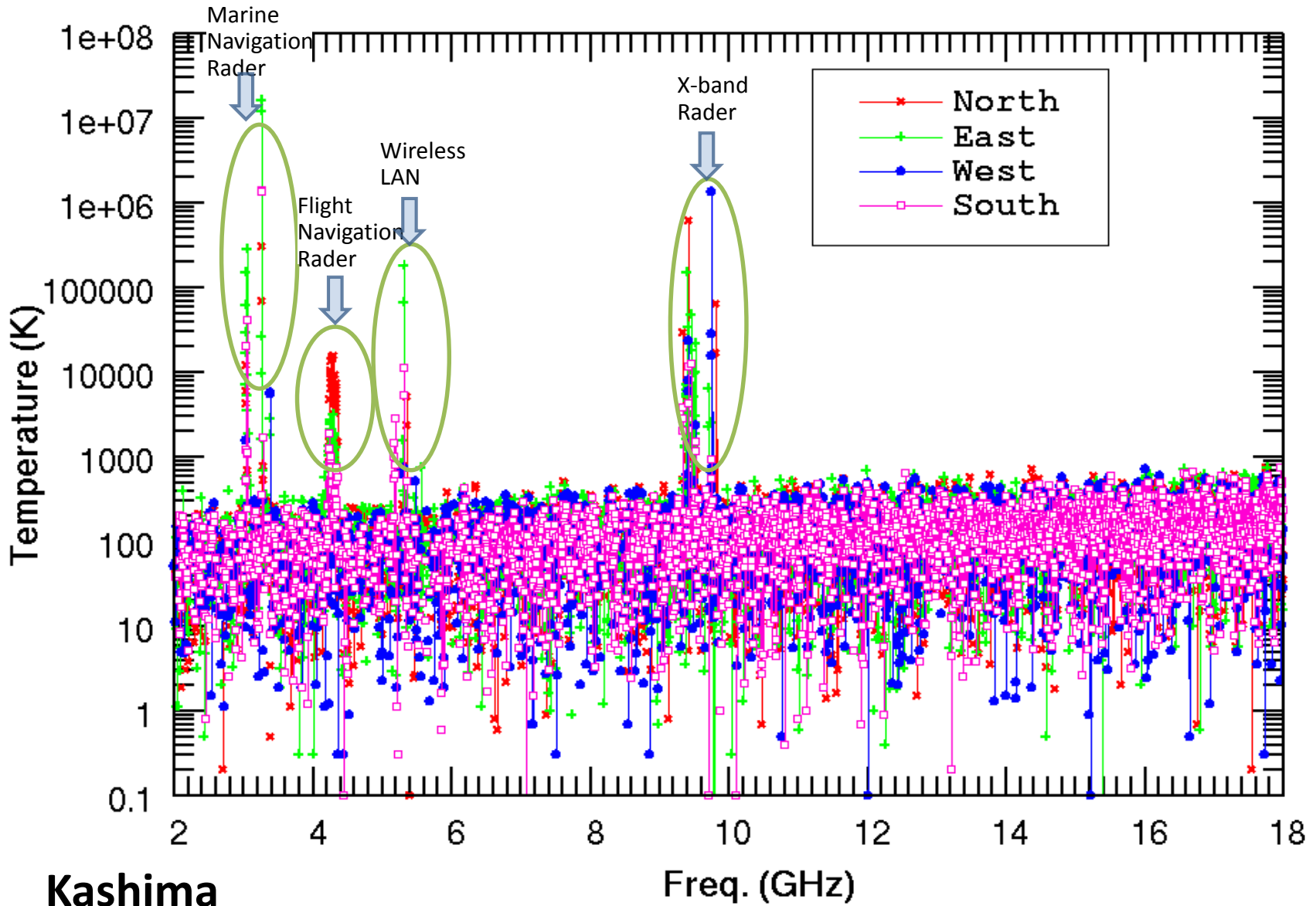


# V/H-Polarization Comparison (NMIJ@Tsukuba)

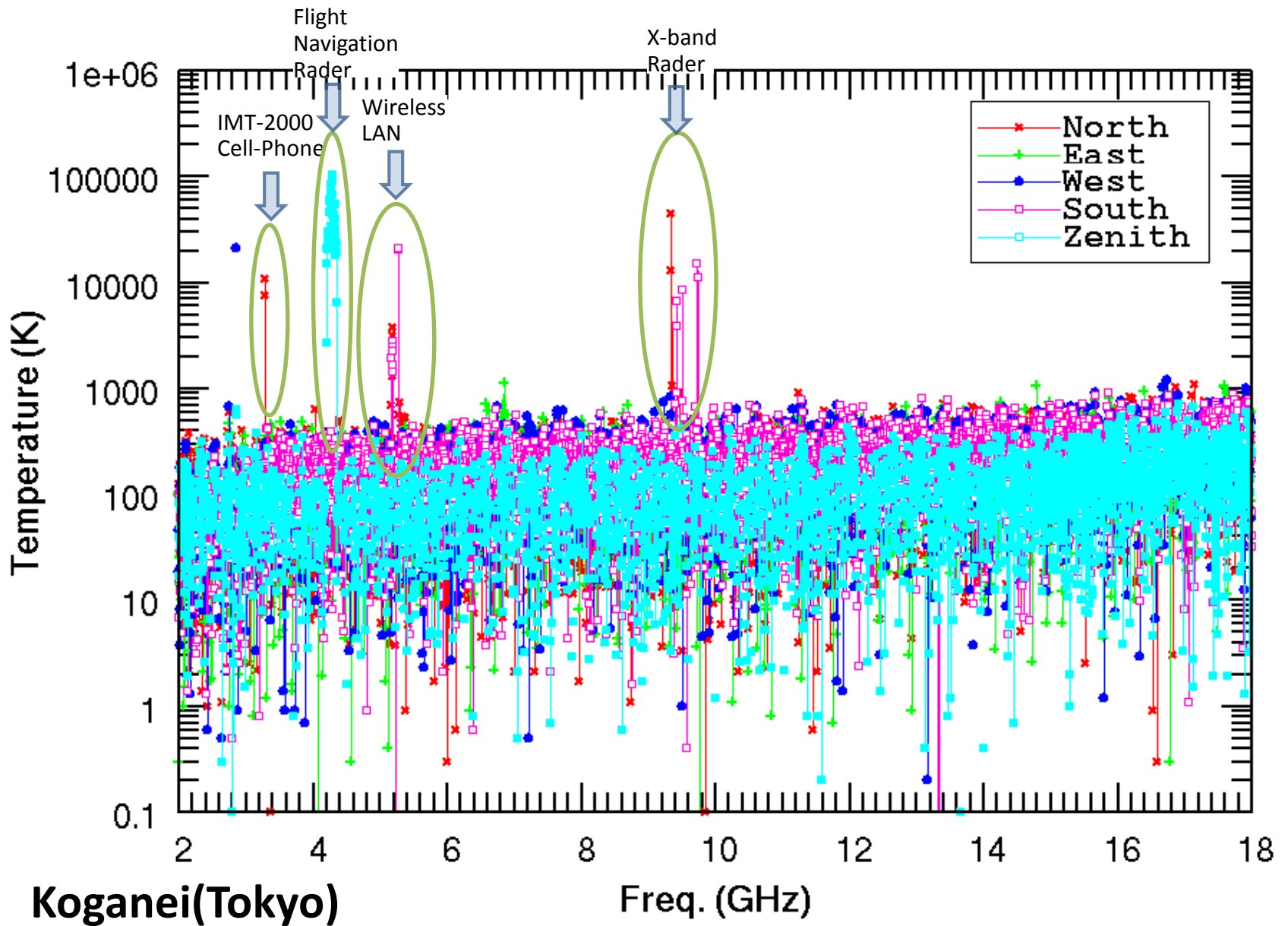
There were no significant difference on V/H Polarization.



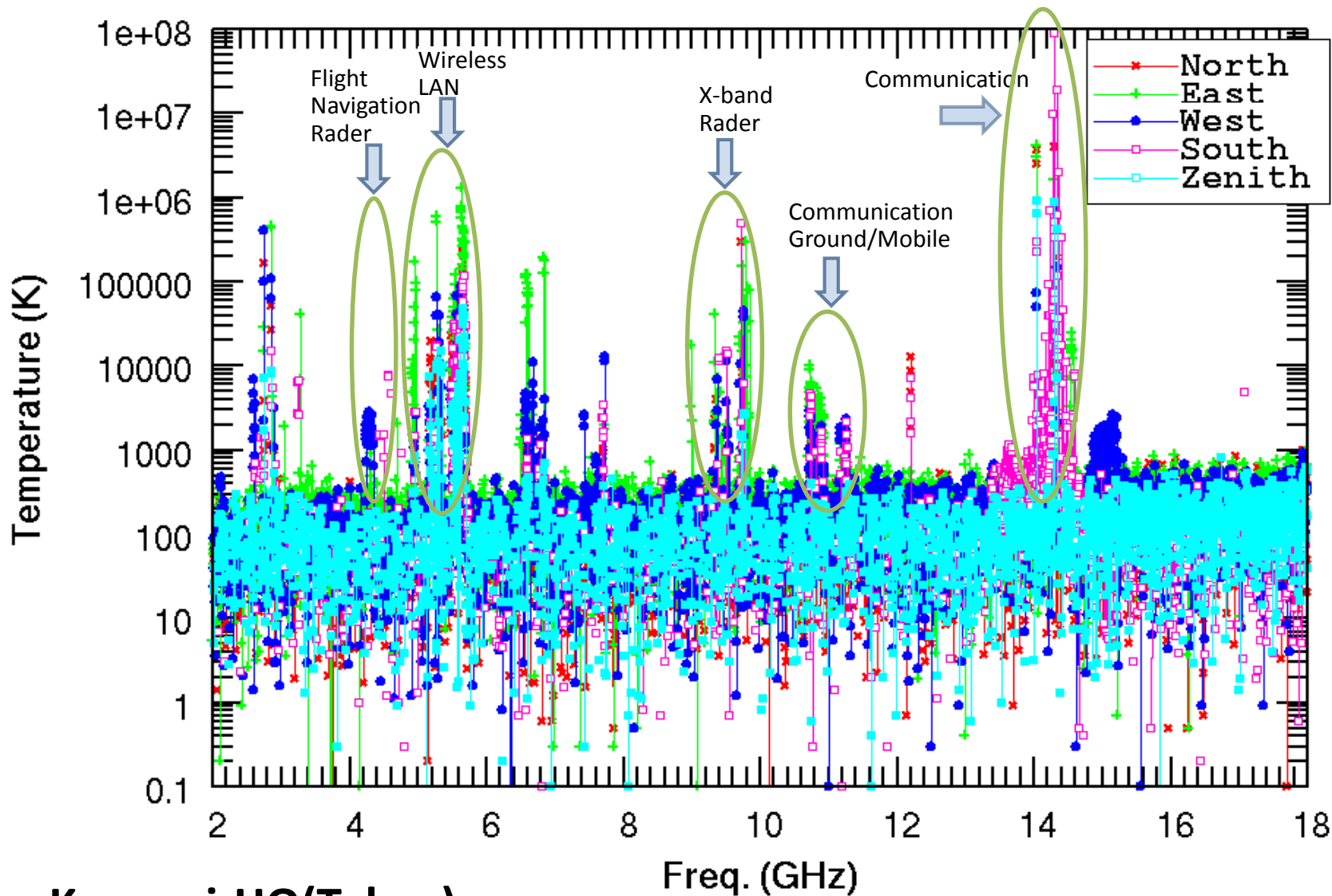
# Speculation of IRF Sources



# Speculation of IRF Sources



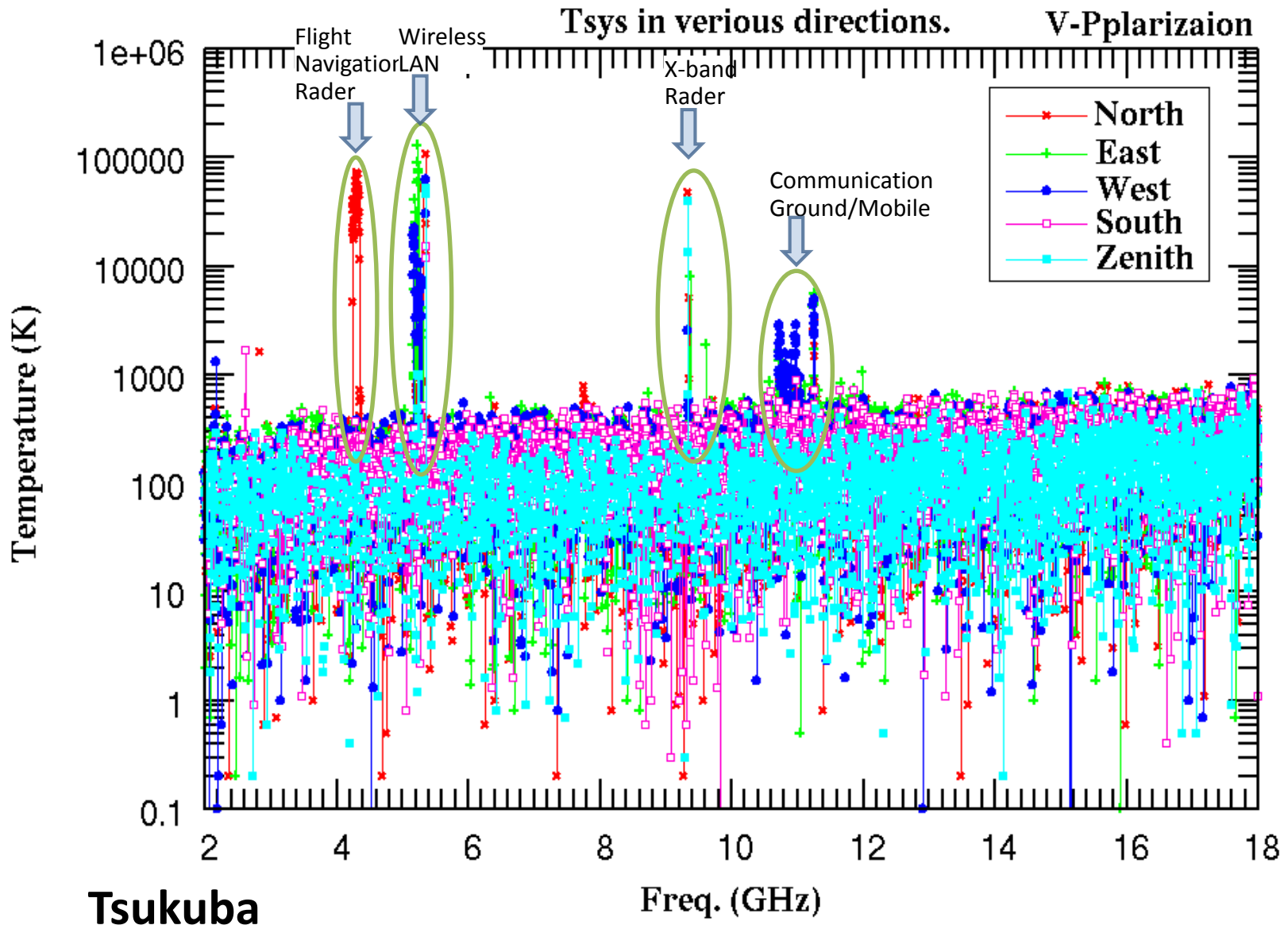
# Speculation of IRF Sources



Koganei-HQ(Tokyo)



# Speculation of IRF Sources



# Sources of RFI

- Cell phone and its base station. (1.48GHz 1.9GHz, 2.2GHz)
- 3.0 - 3.4 GHz: Marine Navigation Rader
- 4.25-4.35 GHz: Flight Navigation Rader (Altimeter)
- 5.15-5.35 GHz: Wireless LAN
- 9.35-9.45, 9.7-9.8 GHz: X-band Rader (Weather, Marine )
- 11.7-12.2 GHz: Broadcasting Satellite
- 12.2-12.75 GHz: Communication Satellite
  - But this may not be so serious since probability of the beam couping is low.
  - But actually it may happen.

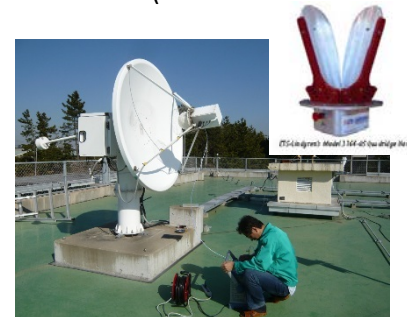
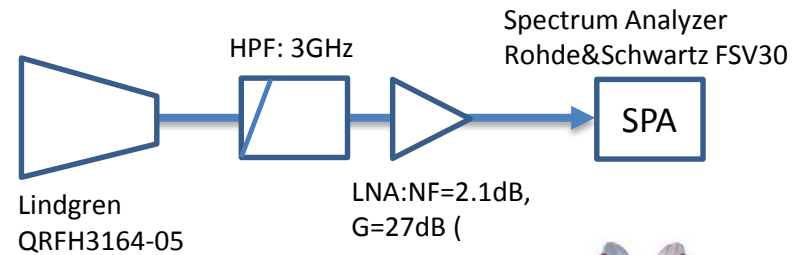
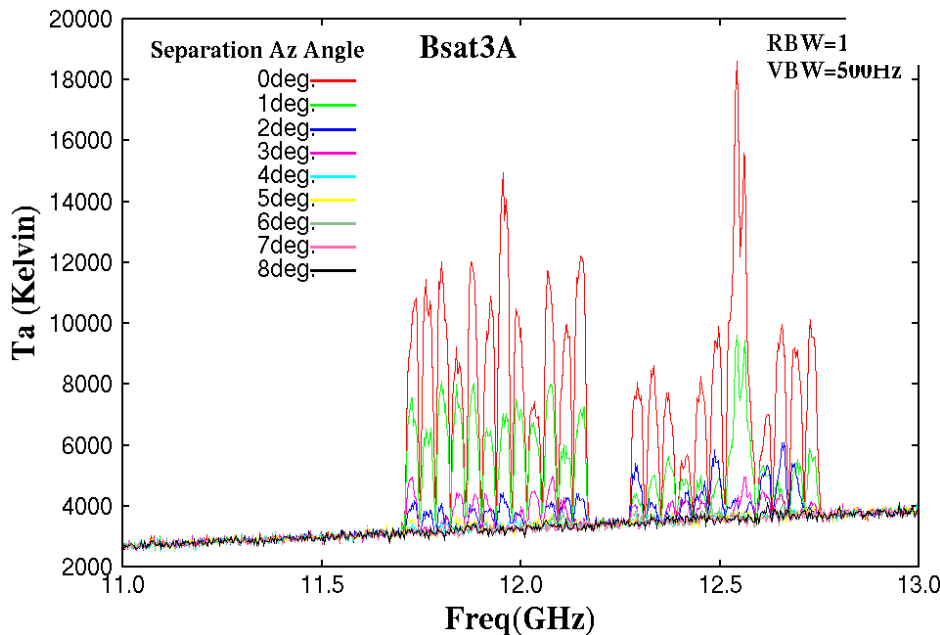
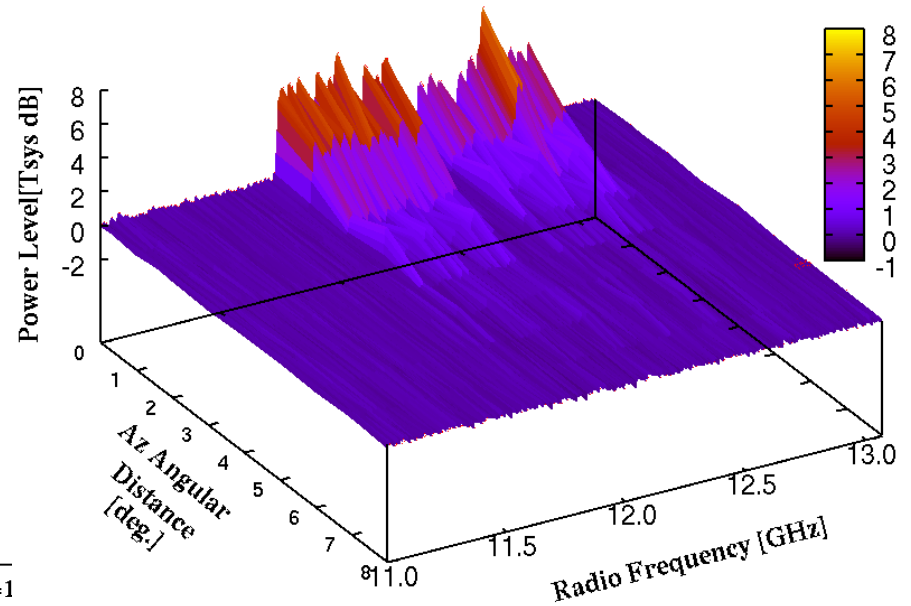
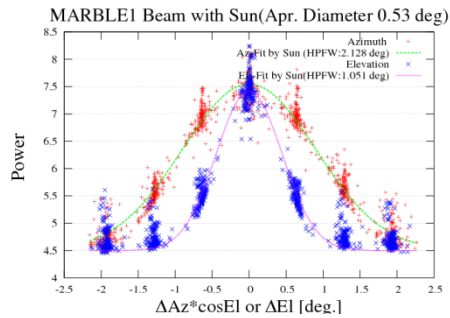
# Influence of RFI from Satellite Signal

Broadcasting Satellite

$$G = \frac{4\pi}{\lambda^2} A\eta$$

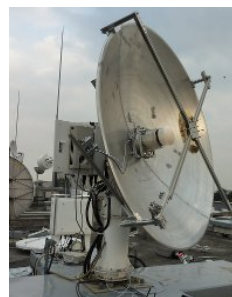
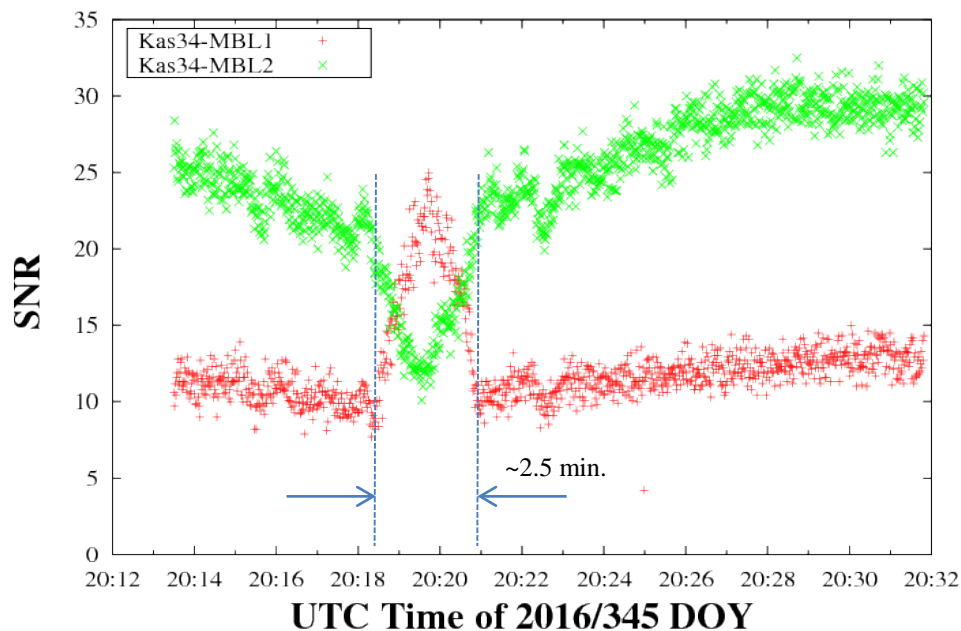
$$\text{Beam Width} = \frac{\lambda}{D}$$

Beam width ~ 2 deg.



# The probability is low but it might have happened!! Pointing to Stellate.

Source: 3C279



Marble2(2.4m)



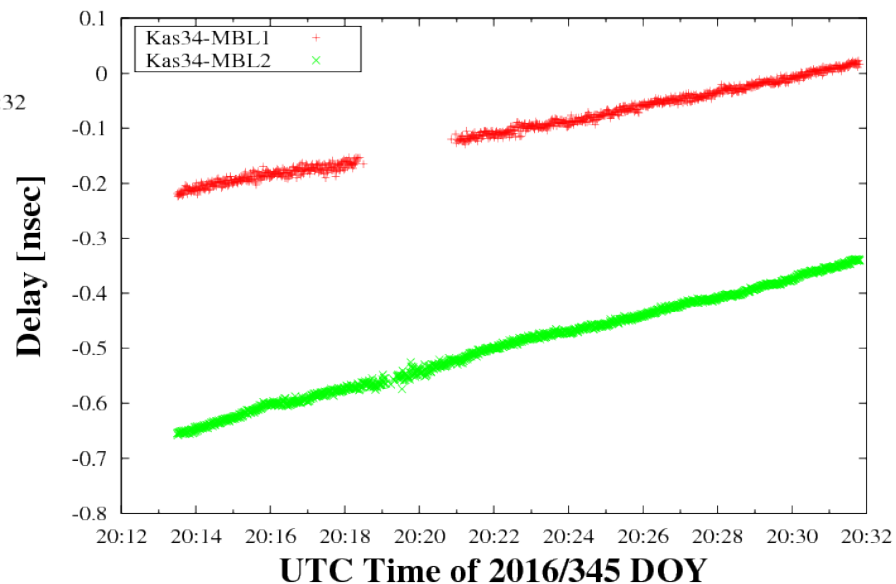
Marble1(1.6m)

Kashima34m

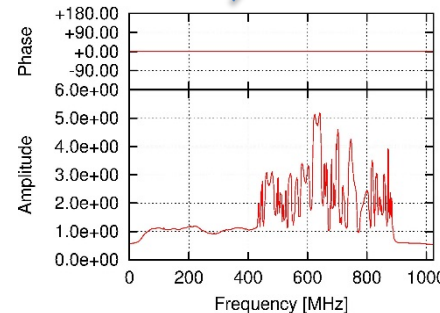
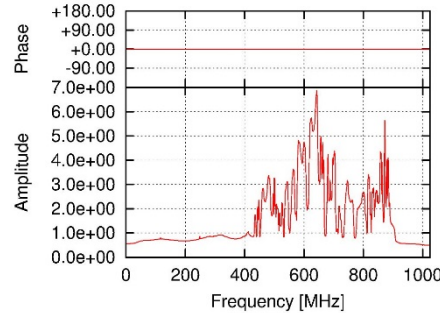
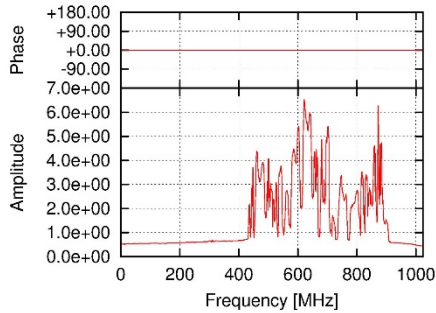
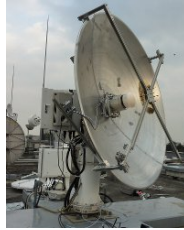
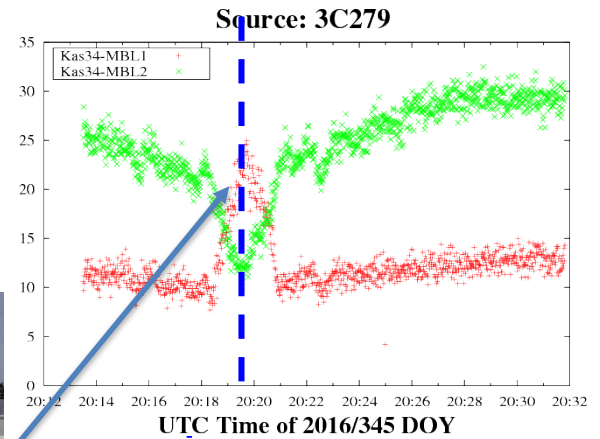


There were abnormal data for a few minutes in output of bandwidth synthesis(3.3-11GHz). Each data points represent observed data with 1 sec. integration.

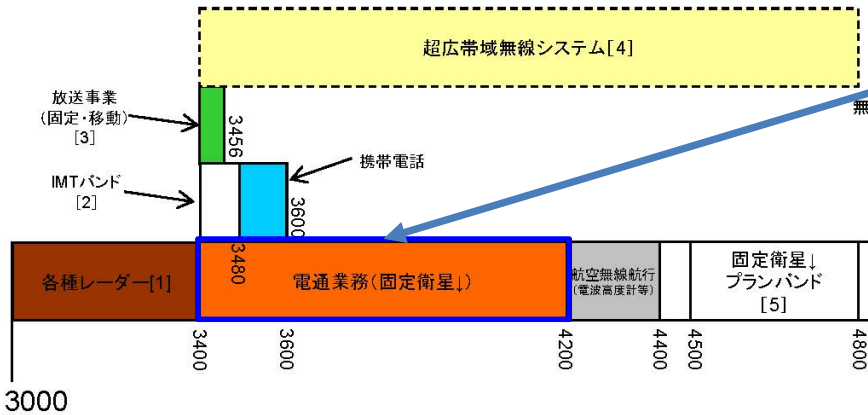
Source: 3C279



# RFI from Satellite



Lo=3288MHz



Downlink from Stationary Satellite

Current Frequency Allocation Table by Ministry of General Affairs.

# Validation of Measurement

## Comparison of Receiving Power between Theory and Practice

### Emission Power of BS Sat.

EIRP=59 dBW for BS  
Prop. Loss= -205.8 dB  
Power on the Earth:-116.8dBm

Beam width~ 1-2 deg.

### Expected Rec. Power

D=1.6m  
 $\eta = 0.4$   
G=42.1 dB

$$G = \frac{4\pi}{\lambda^2} A\eta$$

Power=-74.7dBm

### Actual Rec. Power

T=1.e4 K(-187dBK)  
BW= 400MHz(86dBHz)  
Power=-71.8dBm



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### Expected Rec. Power with VGOS station

D=13m  
 $\eta = 0.6$   
G=62 dB

$$G = \frac{4\pi}{\lambda^2} A\eta$$

Power= -54.8dBm

Expected full receiving power is significant, but beam coupling probability will be much less due to narrow beam width(0.1 deg.)

# A Quiz on Saturation

```

*****
* MONIT (signal level monitor for K5/VSSP | K5/VSSP32 | VSSP64) *
* by T.Kondo/NICT (Ver. 2016-12-14) *
* Target Board is K5/VSSP32 *
*
* CTRL C for STOP *
*
*****T*****KONDO*****

2017/04/13 (103) 11:36:38

2017/04/13 (103) 11:21:32 CH 2 CH 3 CH 4
*
+ FULL |* |** |* |*
|*** |*** |*** |***
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|** |** |** |**
- FULL |* |** |* |*
DC OFFSET 0.8/256 0.3/256 0.5/256 1.0/256
ONE SIGMA 53.0/256 57.7/256 50.9/256 50.9/256
    
```

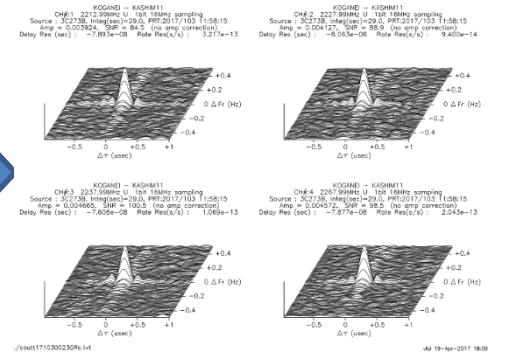


```

*****
* MONIT (signal level monitor for K5/VSSP | K5/VSSP32 | VSSP64) *
* by T.Kondo/NICT (Ver. 2016-12-14) *
* Target Board is K5/VSSP32 *
*
* CTRL C for STOP *
*
*****T*****KONDO*****

2017/04/13 (103) 11:33:54

^C
2017/04/13 (103) 11:21:41 CH 2 CH 3 CH 4
*
+ FULL |** |** |* |*
|*** |*** |*** |***
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|** |** |** |**
- FULL |* |** |* |*
DC OFFSET 1.7/256 0.3/256 0.0/256 -1.2/256
ONE SIGMA 55.1/256 51.1/256 49.0/256 54.8/256
    
```



```

*****
* MONIT (signal level monitor for K5/VSSP | K5/VSSP32 | VSSP64) *
* by T.Kondo/NICT (Ver. 2016-12-14) *
* Target Board is K5/VSSP32 *
*
* CTRL C for STOP *
*
*****T*****KONDO*****

2017/04/13 (103) 12:03:03

^C
2017/04/13 (103) 12:00:42 CH 2 CH 3 CH 4
*
+ FULL |***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|** |** |** |**
- FULL |***** |***** |***** |*****
DC OFFSET -0.5/256 -0.7/256 -0.8/256 -0.2/256
ONE SIGMA 76.3/256 72.3/256 73.4/256 73.7/256
    
```

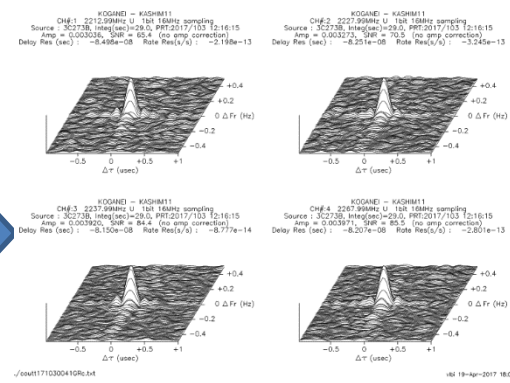


```

*****
* MONIT (signal level monitor for K5/VSSP | K5/VSSP32 | VSSP64) *
* by T.Kondo/NICT (Ver. 2016-12-14) *
* Target Board is K5/VSSP32 *
*
* CTRL C for STOP *
*
*****T*****KONDO*****

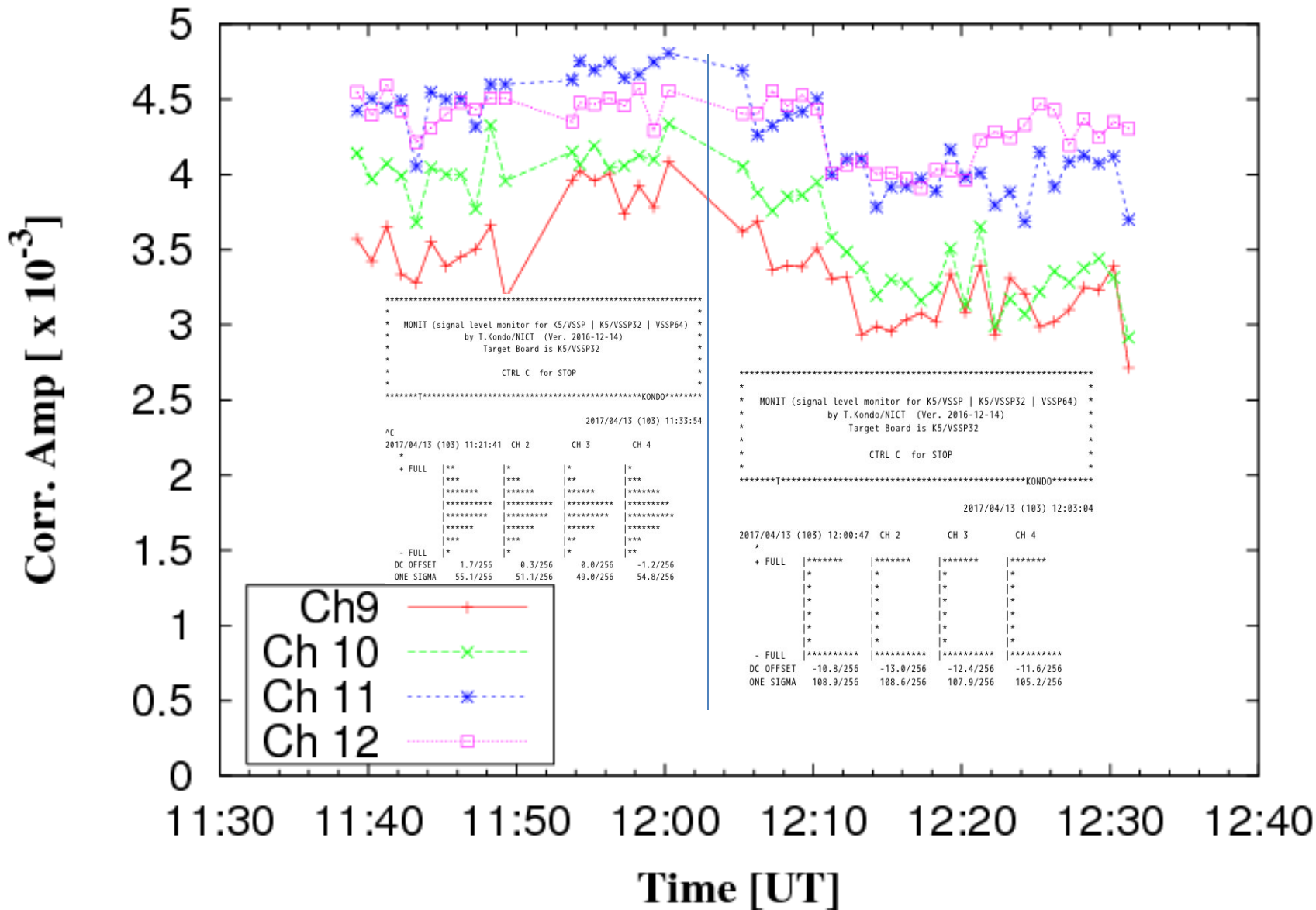
2017/04/13 (103) 12:03:04

2017/04/13 (103) 12:00:47 CH 2 CH 3 CH 4
*
+ FULL |***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|***** |***** |***** |*****
|** |** |** |**
- FULL |***** |***** |***** |*****
DC OFFSET -10.8/256 -13.0/256 -12.4/256 -11.6/256
ONE SIGMA 108.9/256 108.6/256 107.9/256 105.2/256
    
```



# Saturation is not problem for 1bit sampling

Decrease of Corr. Amp is due to Loss of Info caused by DC-bias, but not saturation.

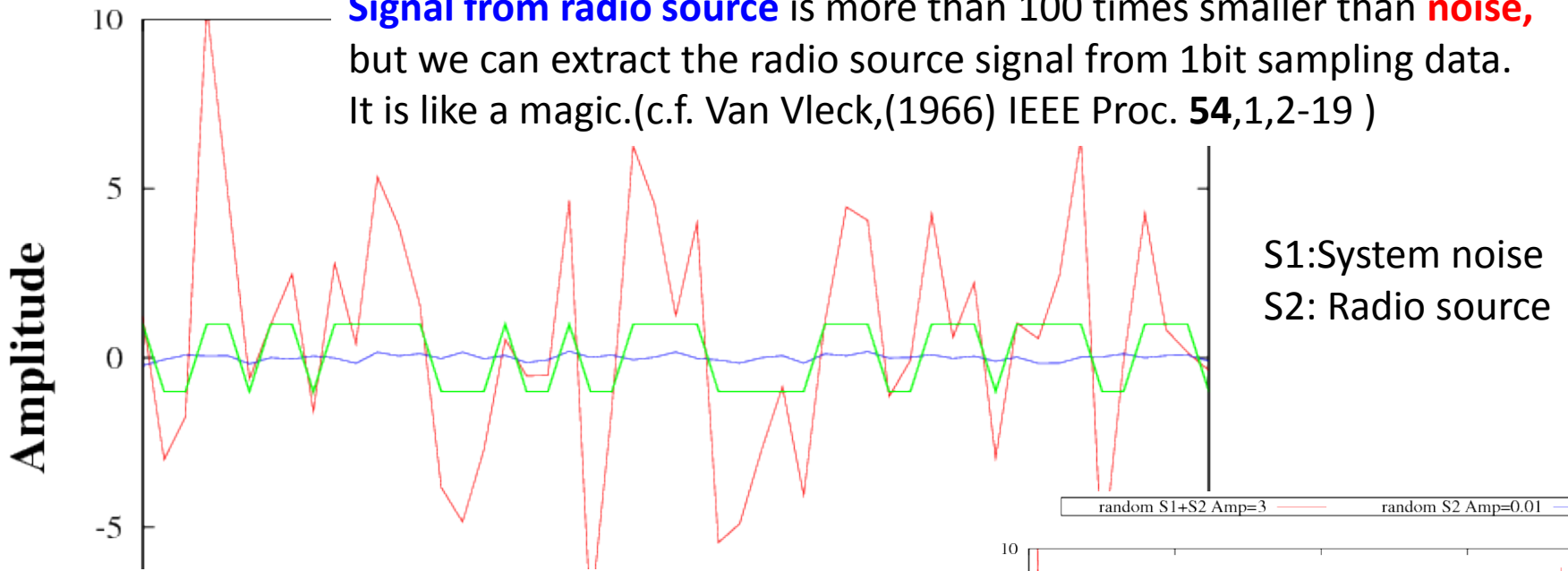




# 1bit sampling Simulation [noise(3)]



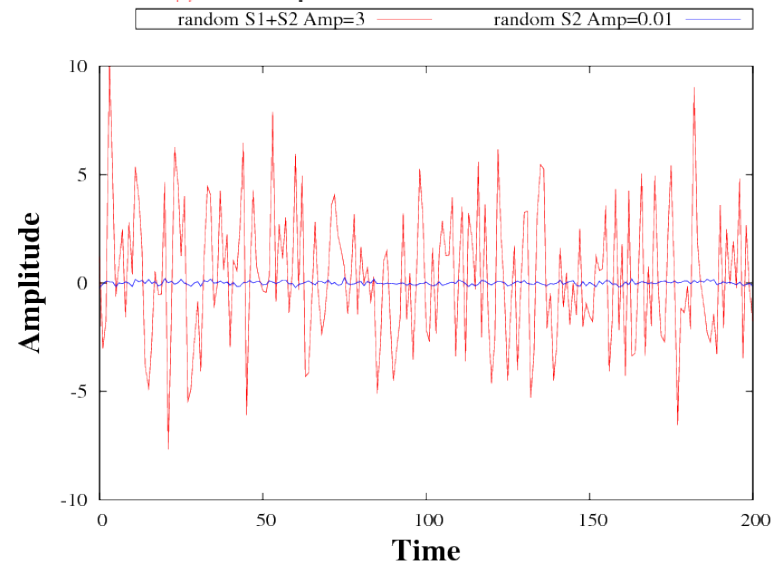
**Signal from radio source** is more than 100 times smaller than **noise**, but we can extract the radio source signal from 1bit sampling data. It is like a magic.(c.f. Van Vleck,(1966) IEEE Proc. **54**,1,2-19 )



It works under the condition [Corr. Amp << 1] and each samples are independent each other.

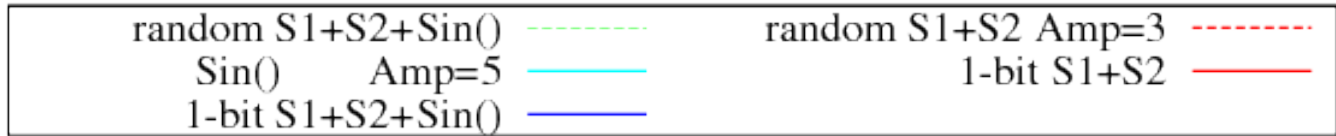


VLBI(1bit) is sampling the probability distribution of the signal.

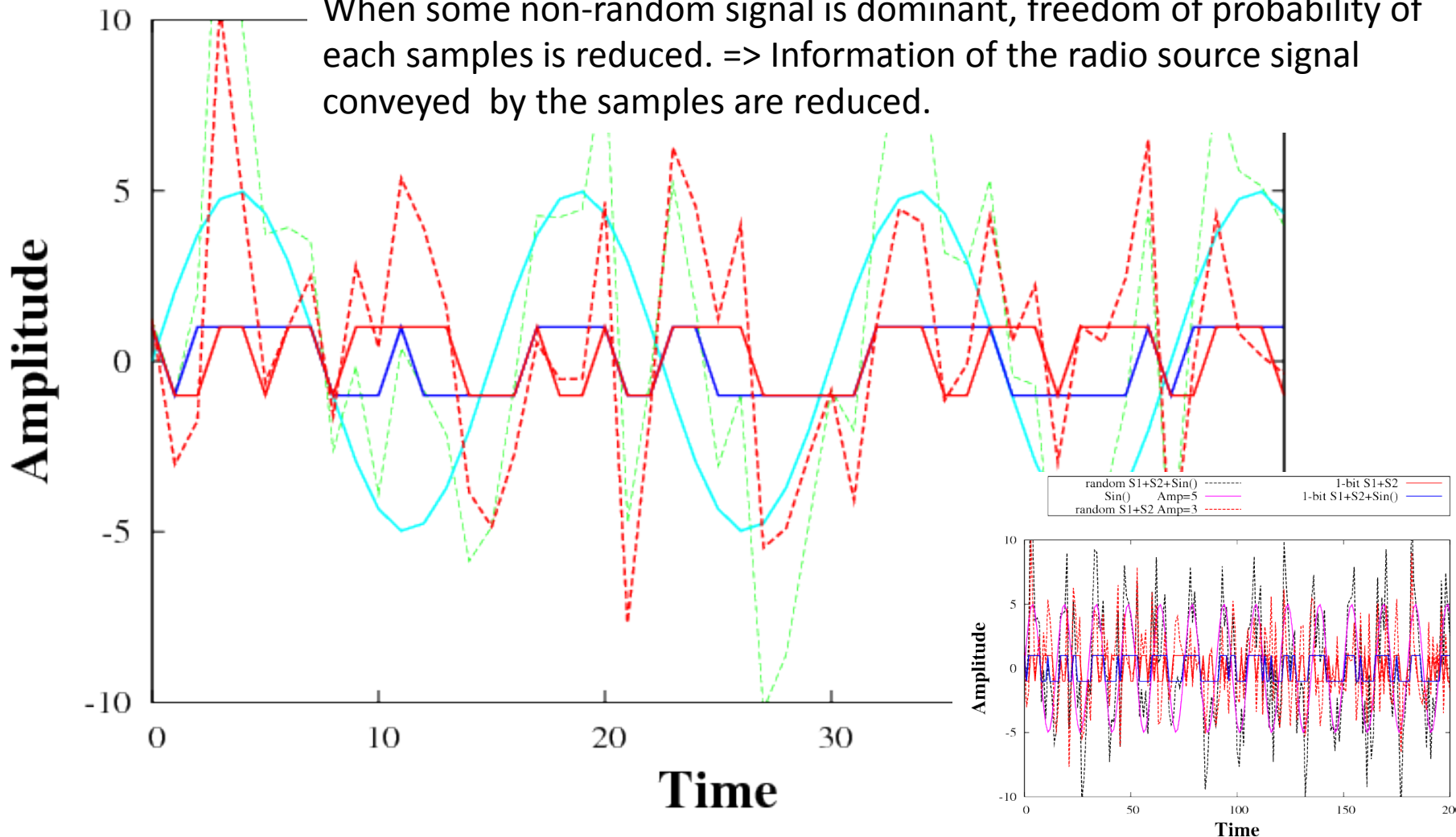


# 1bit sampling Simulation [noise(3)+sin(5)]

S1: System noise  
S2: Radio source



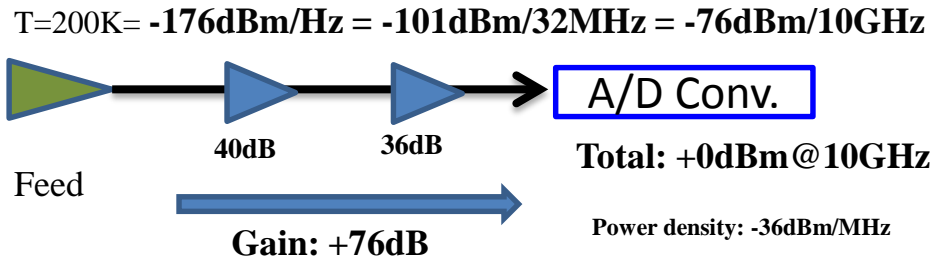
When some non-random signal is dominant, freedom of probability of each samples is reduced. => Information of the radio source signal conveyed by the samples are reduced.



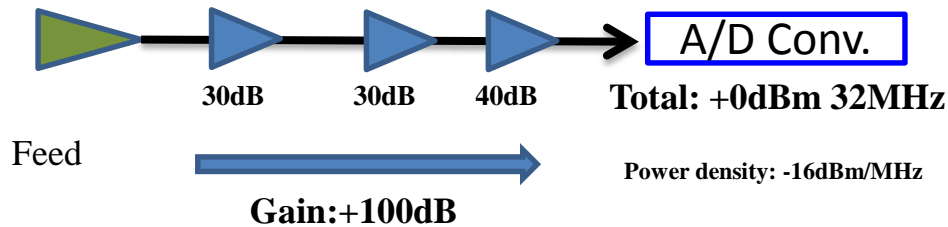
# Advantage of RF-Direct Sampling

## - Robustness to RFI -

### Broadband (~ 10GHz) Case:



### Narrow Band (~ 32MHz) Case:

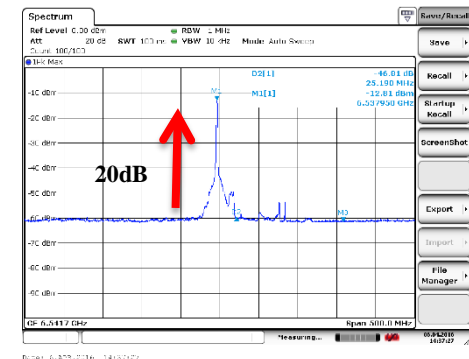


### Case Study:

In the case RFI of +20dB up from noise floor with 1 MHz width (= -96dBm).

Total Power of RFI	<	Total Power of Signal
<b>-20dBm</b>		<b>0dBm</b>

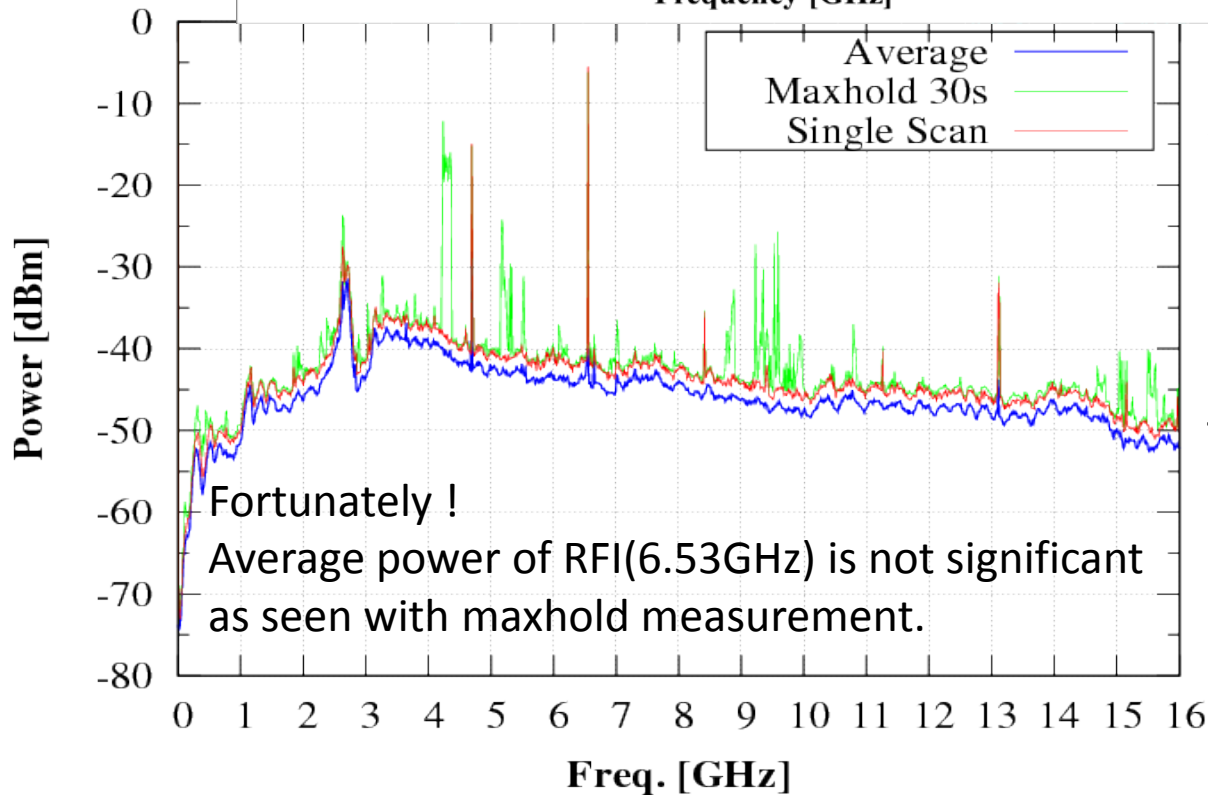
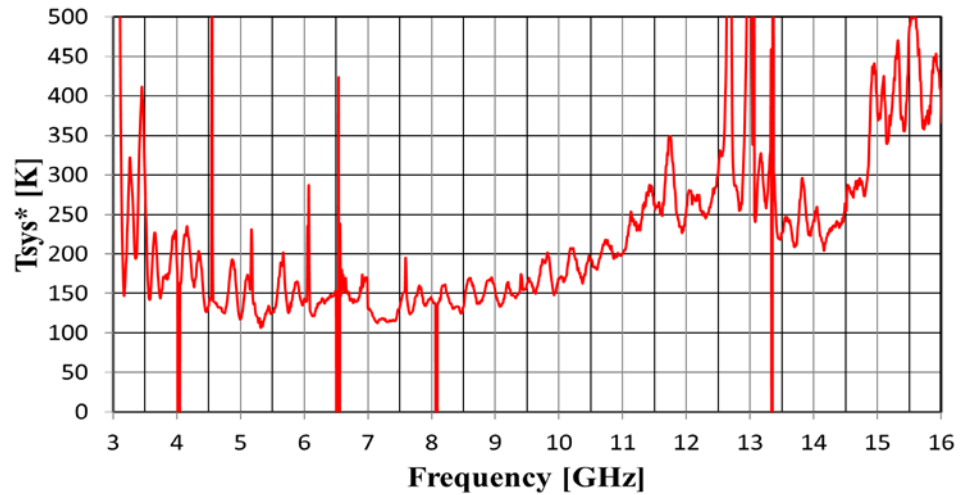
Total Power of RFI	>	Total Power of Signal
<b>+5dBm</b>		<b>0dBm</b>



# Current

## Kashima 34m

# 34m



RBW=3MHz  
Whole BW~12GHz

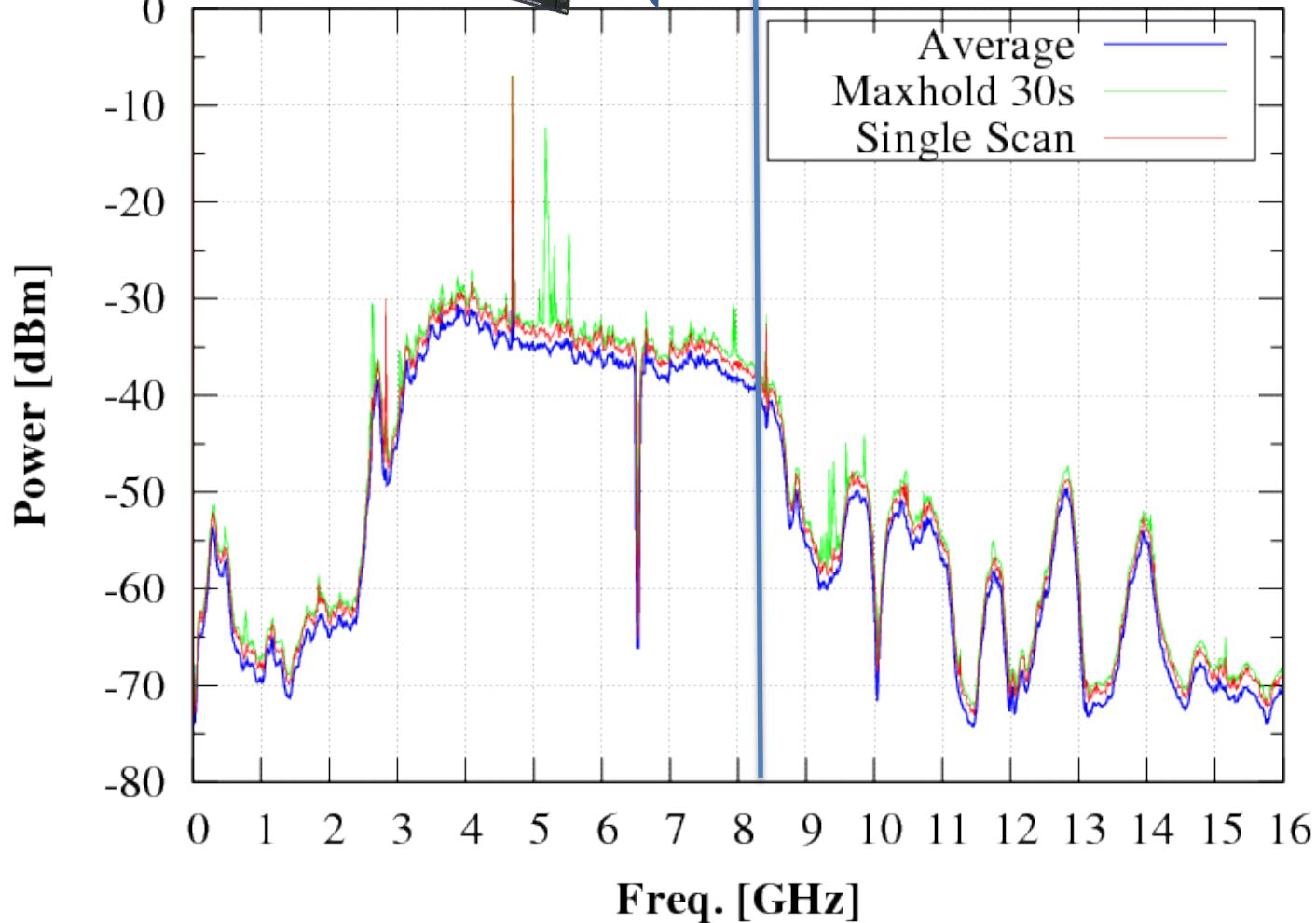
$N=12\text{GHz}/3\text{MHz}$   
=36dB

Total Power~-45+36  
=-9dBm  
< -5dBm (RFI)

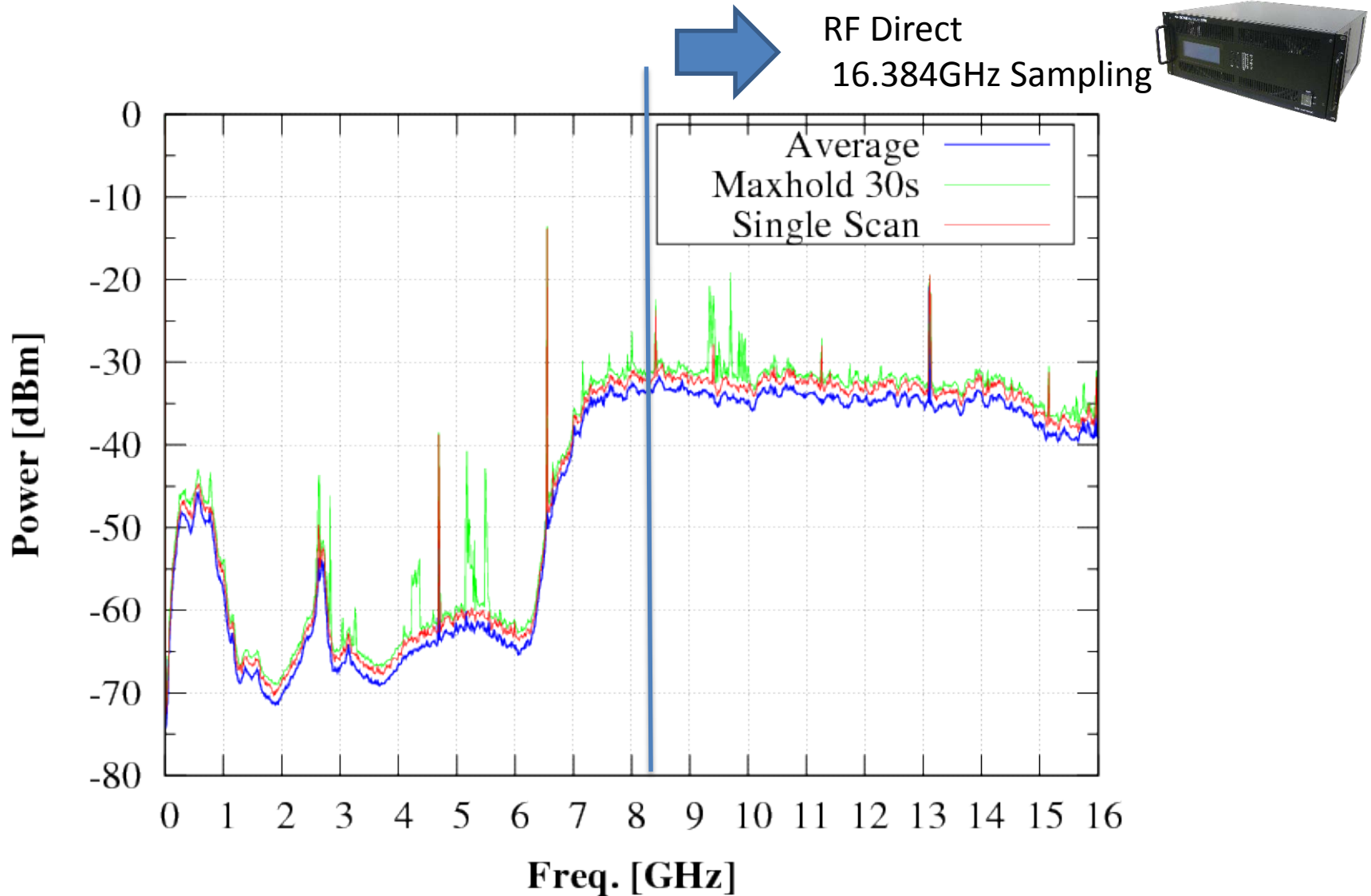
# Real Input to A/D at Kashima 34m Broadband Signal(Lower Band<8.2GHz)

RF Direct

16.384 GHz Sampling



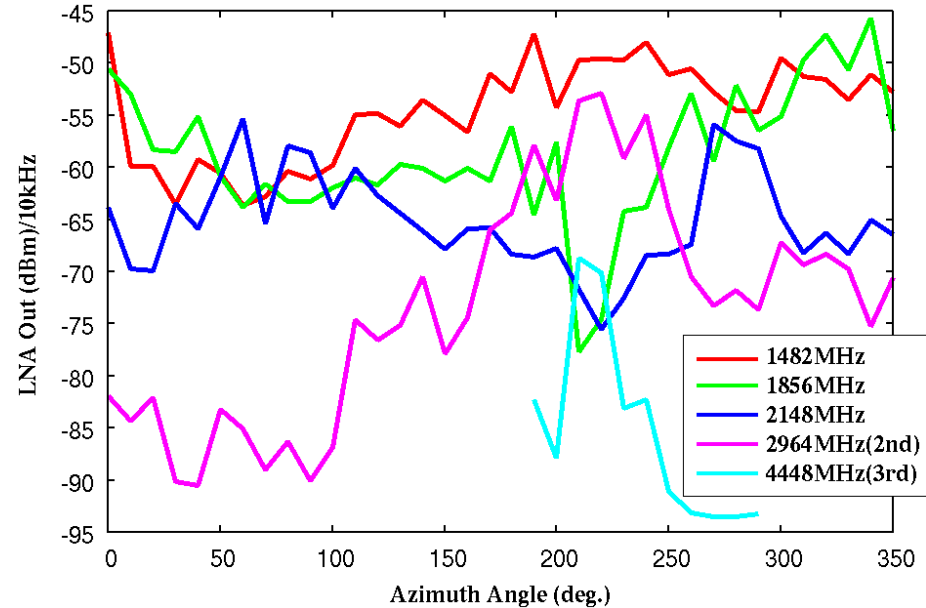
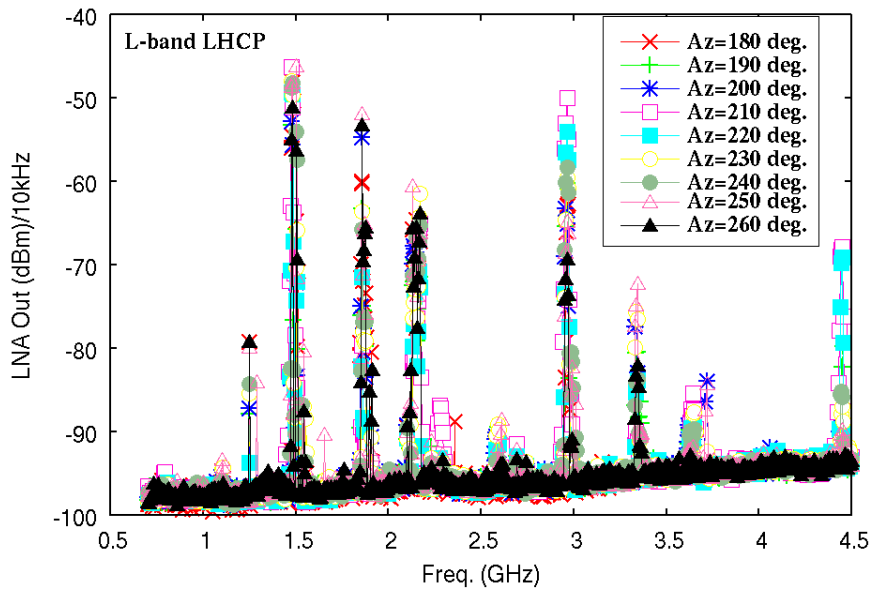
# Real Input to A/D at Kashima 34m Broadband Signal(Upper Band >8.2GHz)



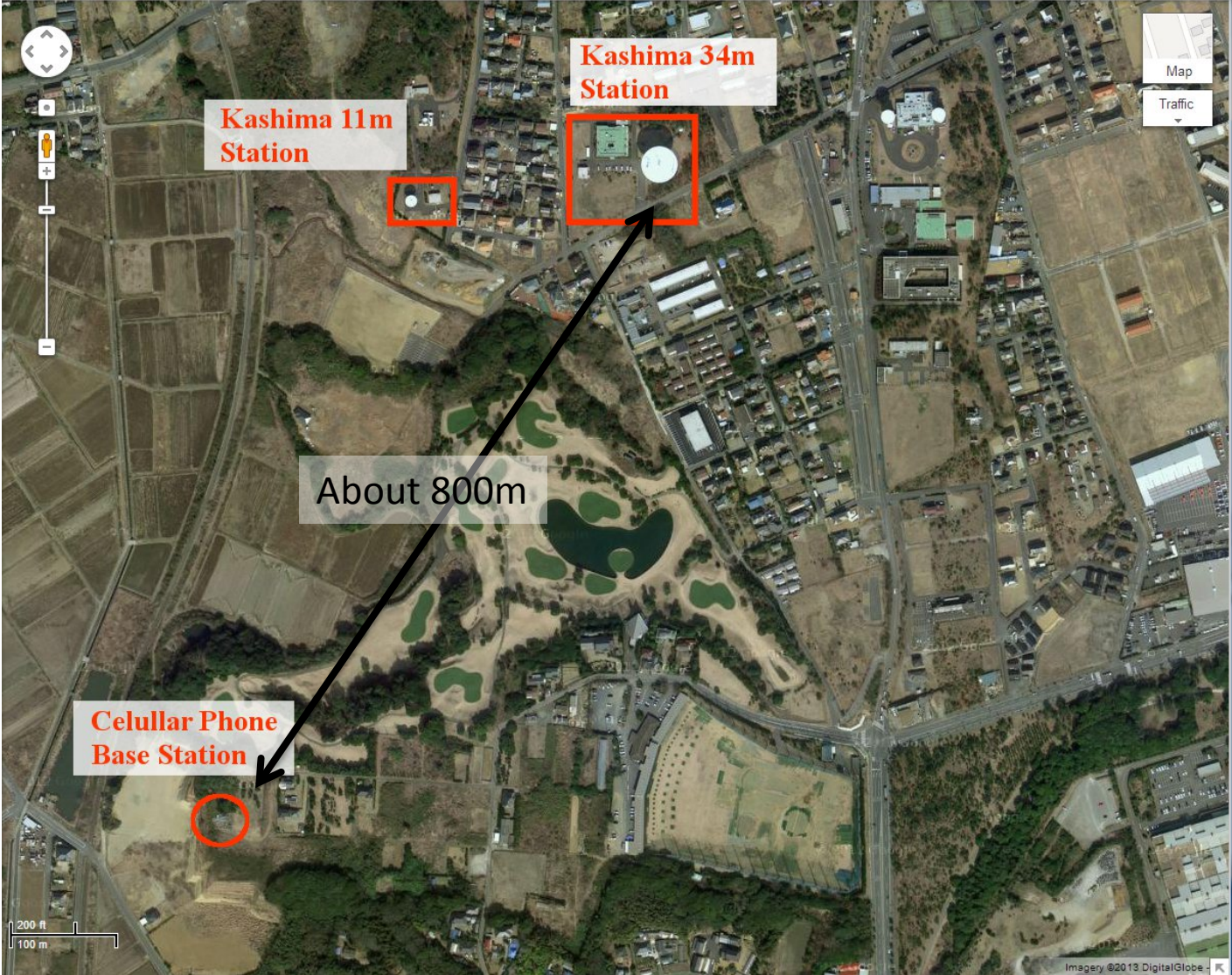
# Example of a LNA saturation due to strong RFI



- L-band receiver of Kashima 34m Radio Telescope was affected



# Source of RFI (Cell Phone Base Station)



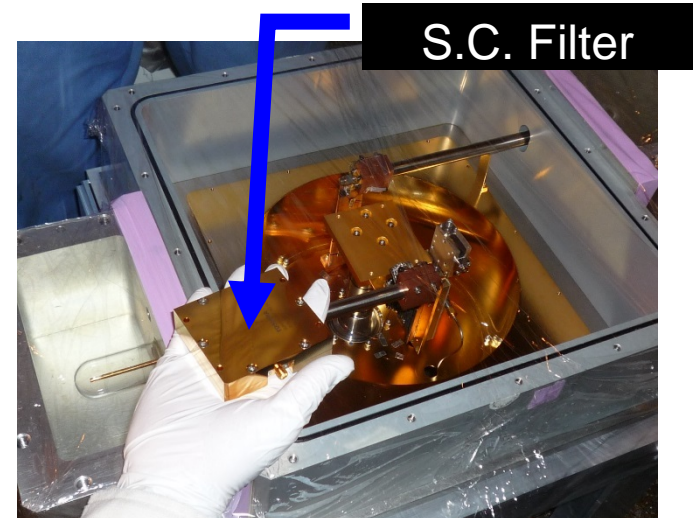
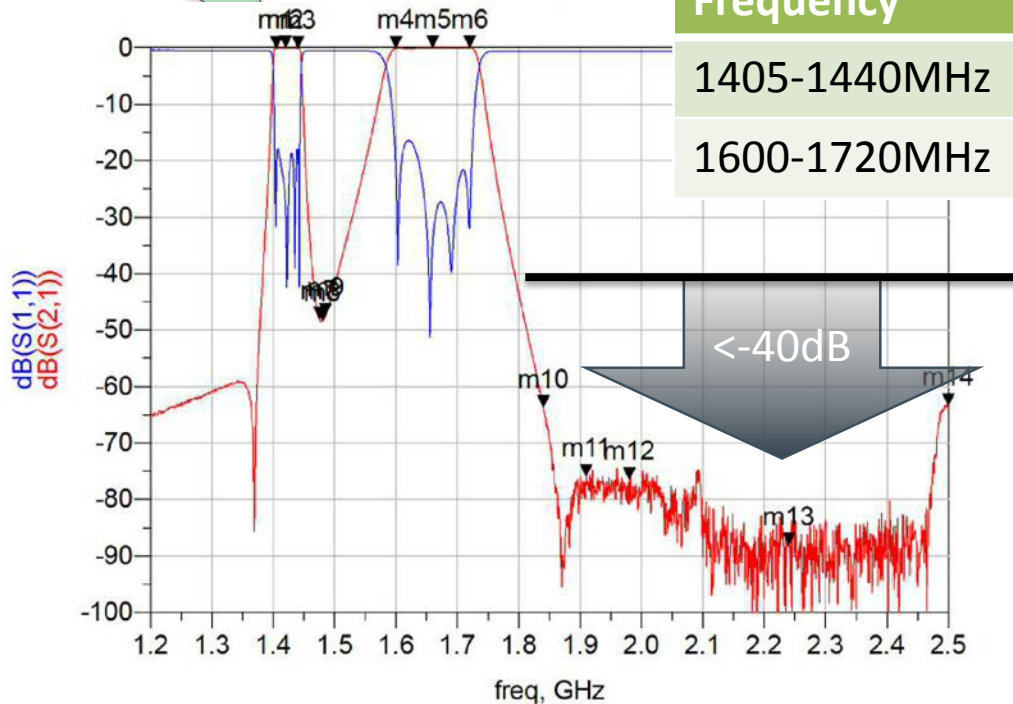


# We could solve the problem

- Super Conductor Filter(Toshiba Co. Ltd) in front of LNA.
- By negotiation with Cell Phone carrier Company, they paid for the filter cost(~87k USD).

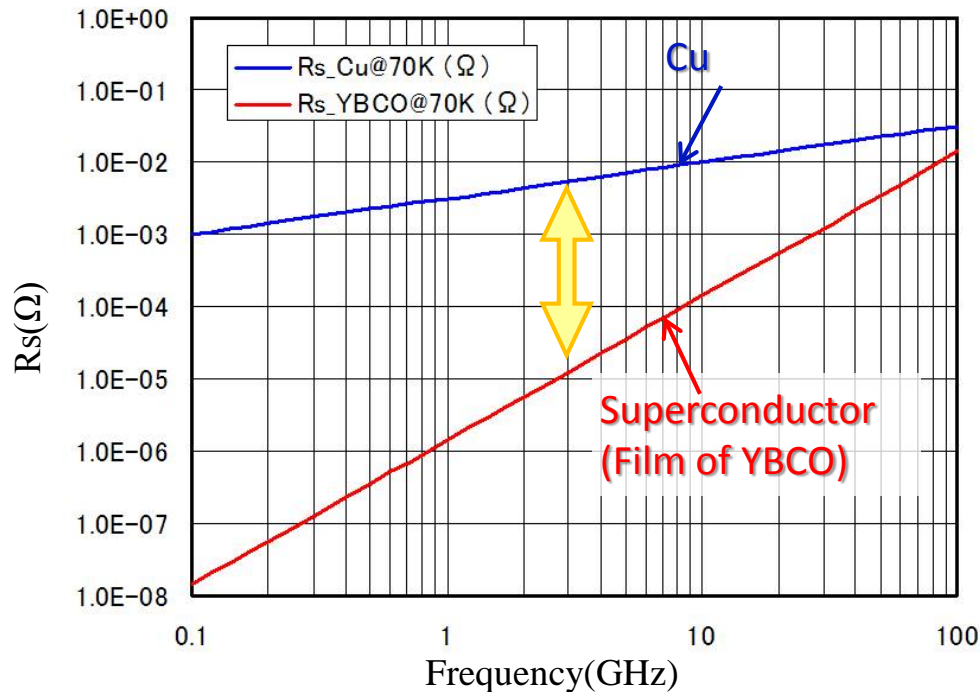
Insertion Loss < 0.5dB

Pass band Frequency	Insertion Loss@20K	Additive Noise [K]
1405-1440MHz	<0.12dB	<0.6 K
1600-1720MHz	<0.08 dB	<0.4K



# Background

- Superconducting materials have low surface resistance characteristic.



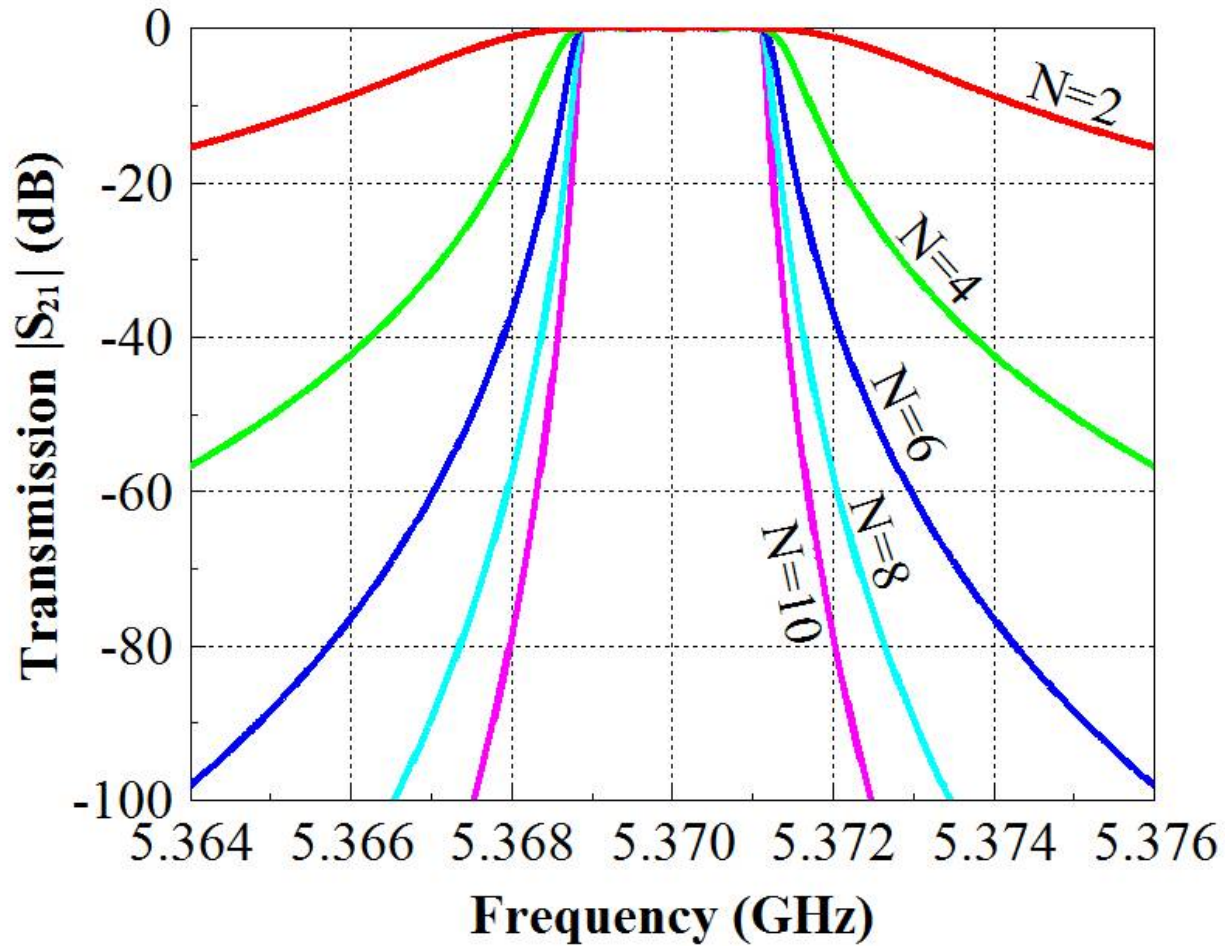
Superconductor is three orders of lower  $R_s$  as compared to copper

\* 1 YBCO:  $YBa_2Cu_3O_{7-x}$

## Surface resistance characteristic of Superconducting film (YBCO \* 1)

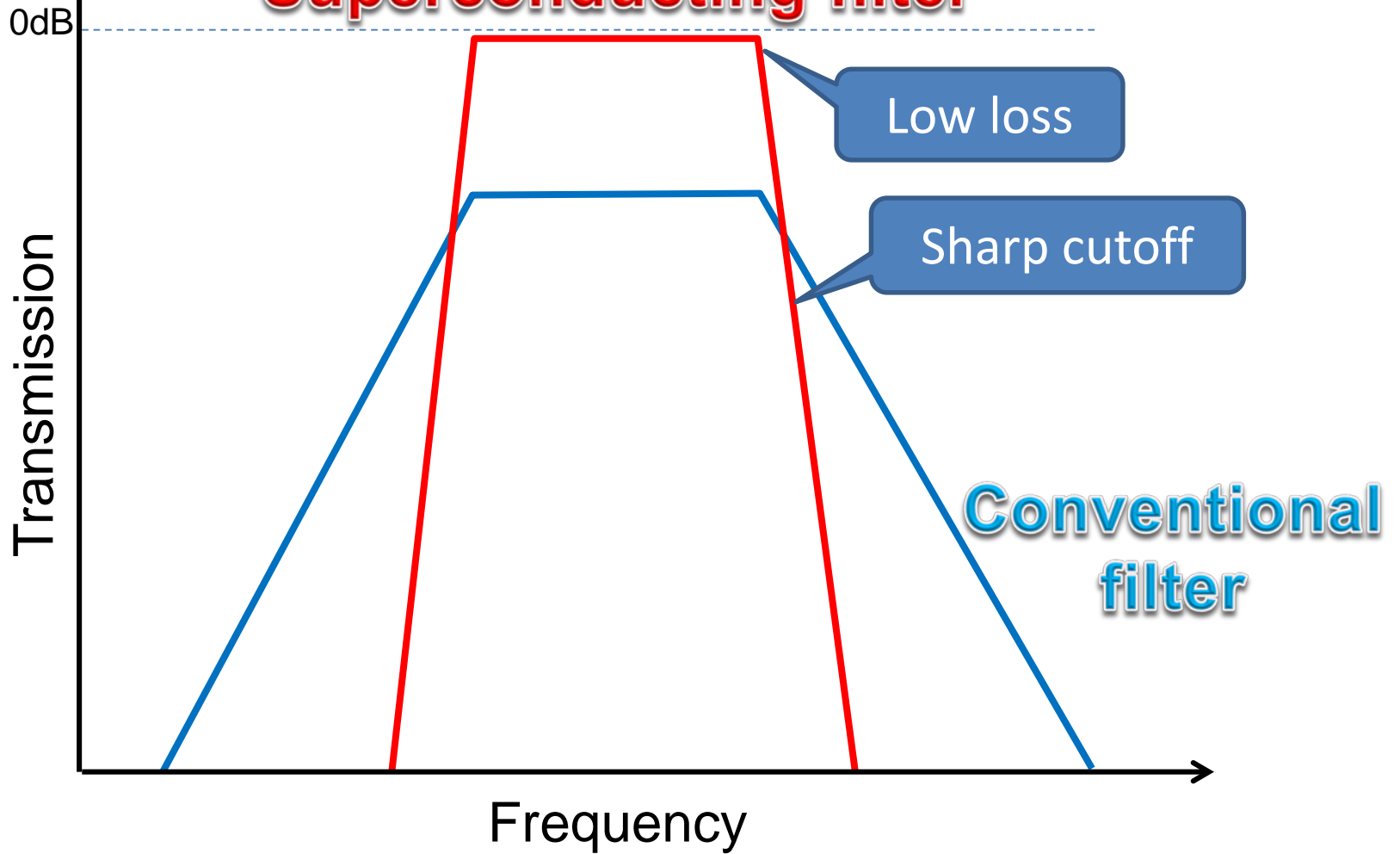
T.Hashimoto, et al., IEICE Trans. Electron., vol. E86-C, No. 8, pp. 1721-1728, Aug. 2003.

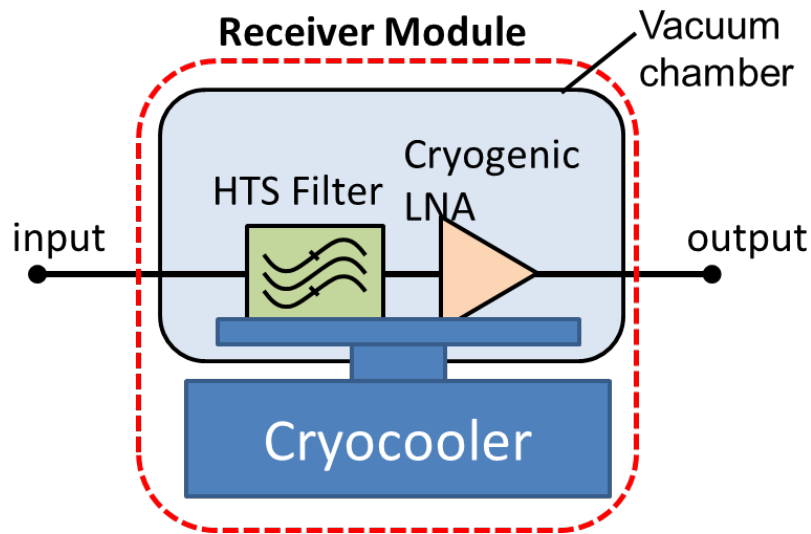
# Dependence of Resonator Number



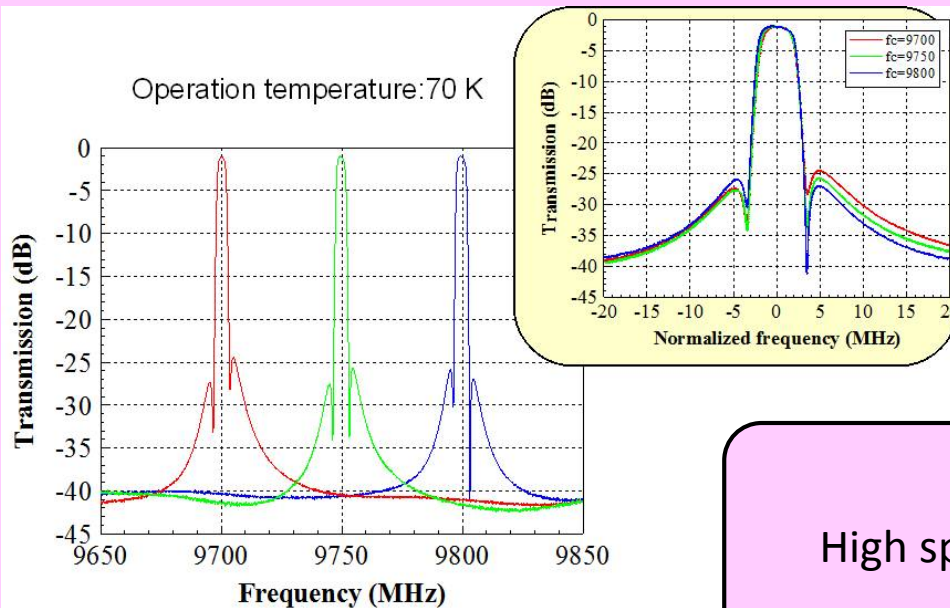
# Merit of Superconducting Filter

**Superconducting filter**





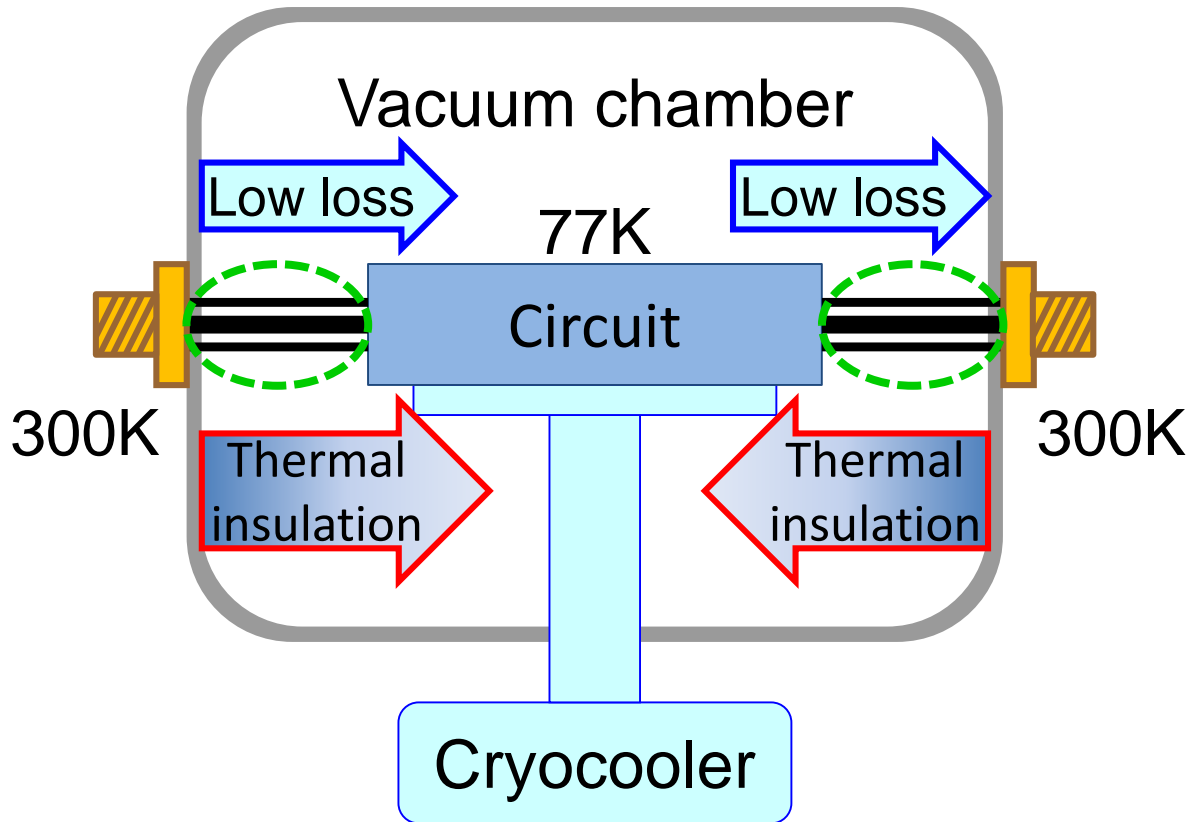
2L size receiver unit at 77 K cooled by Starling cycle cryogenic system.



**Tunable**

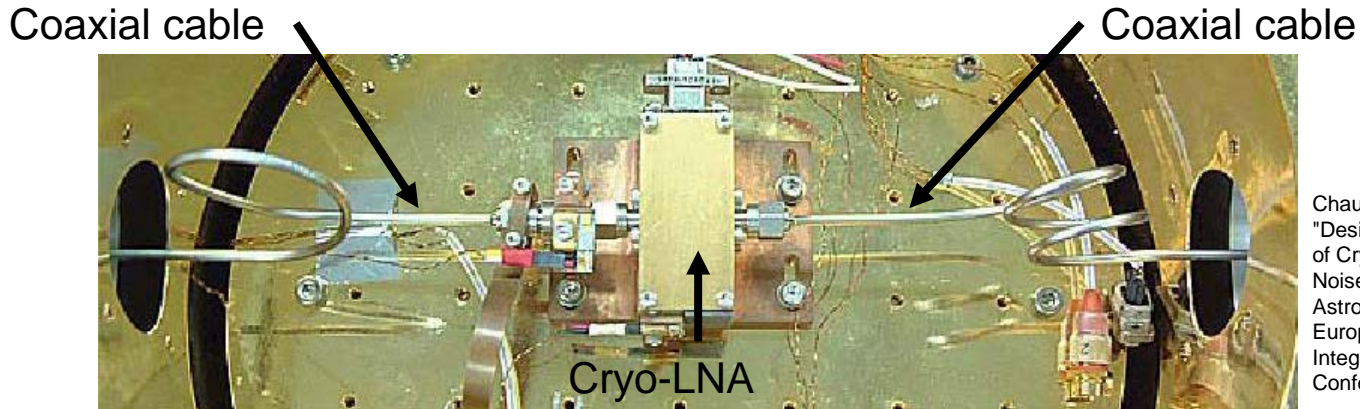
High speed and constant bandwidth

# Thermal Insulating RF interface



Compatibility of both low loss and thermal insulation

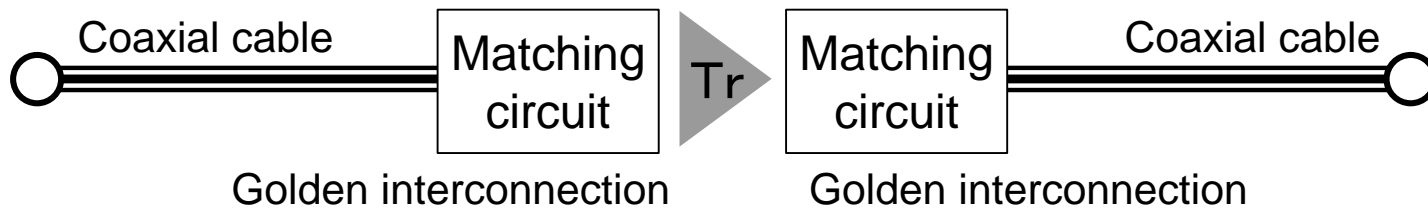
# RF interface Comparison



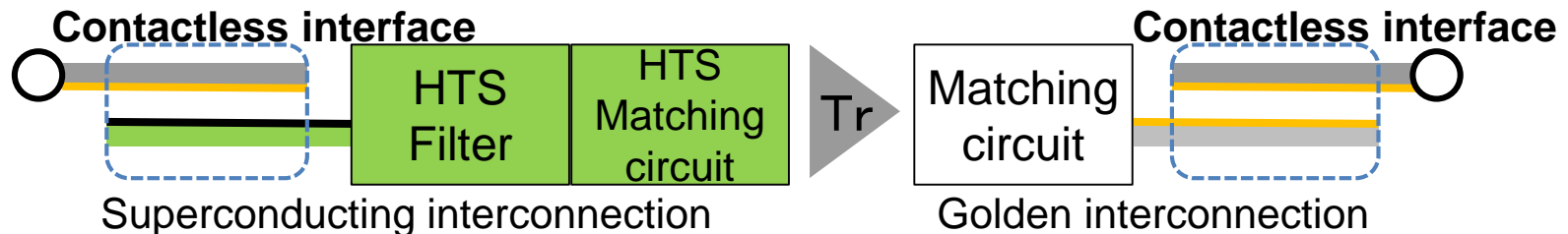
Chau-Ching Chiong, et. al,  
"Design and Measurements  
of Cryogenic MHEMT IF Low  
Noise Amplifier for Radio  
Astronomical Receivers," 4th  
European Microwave  
Integrated Circuits  
Conference, Sept. 2009.

Require the large cryocooler for large thermal conduction

## ● Conventional technique



## ● New technique

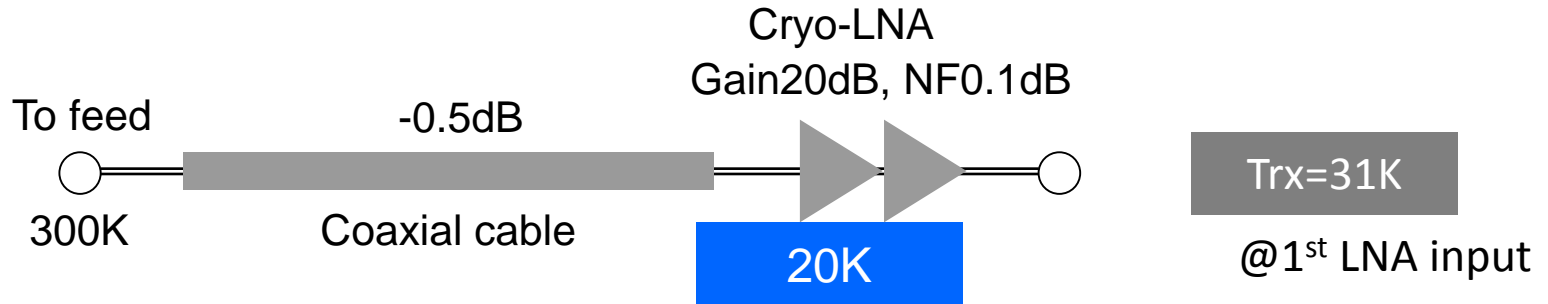


# **Example of installation to Usuda 64 m radio telescope**

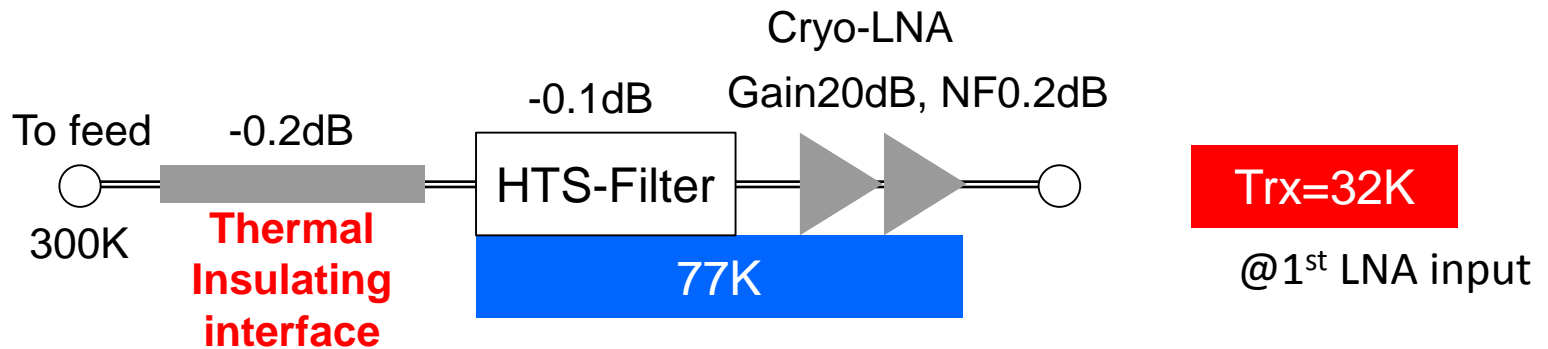


# Comparison of Receiver Noise Temperature

## ● Conventional Cryo-receiver



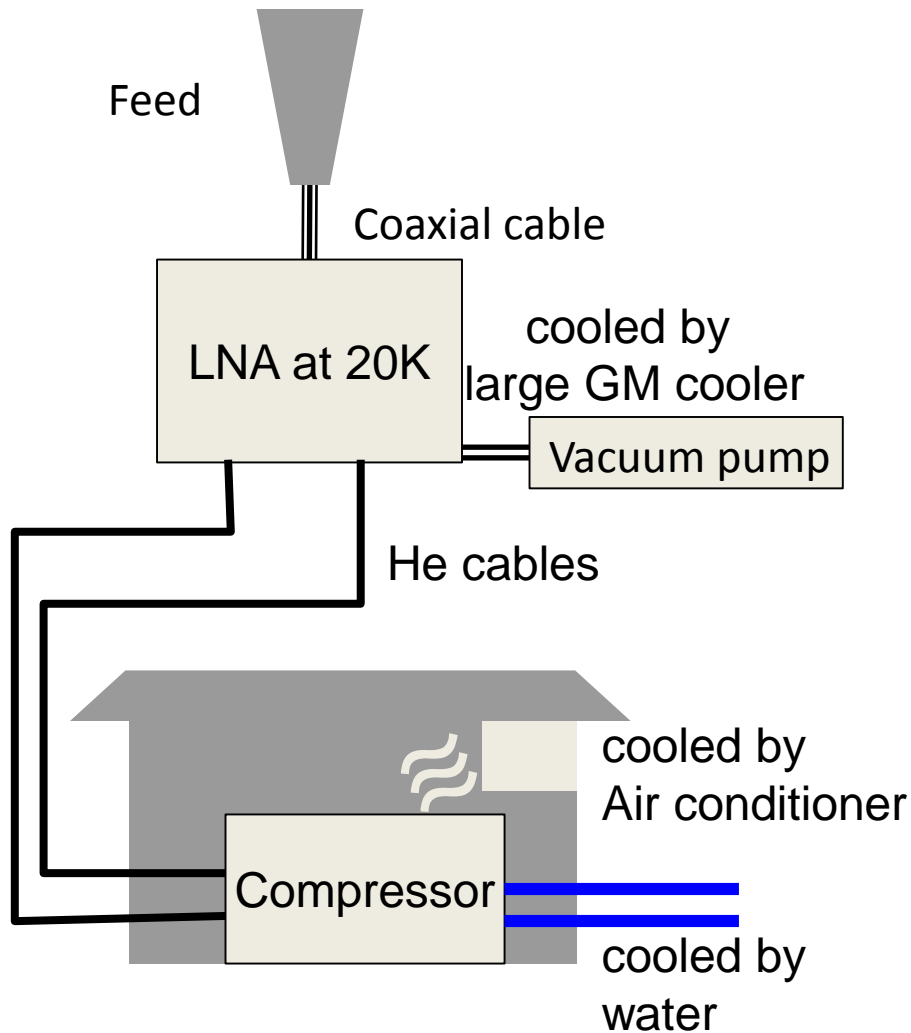
## ● Cryo-receiver with thermal insulating interface technique



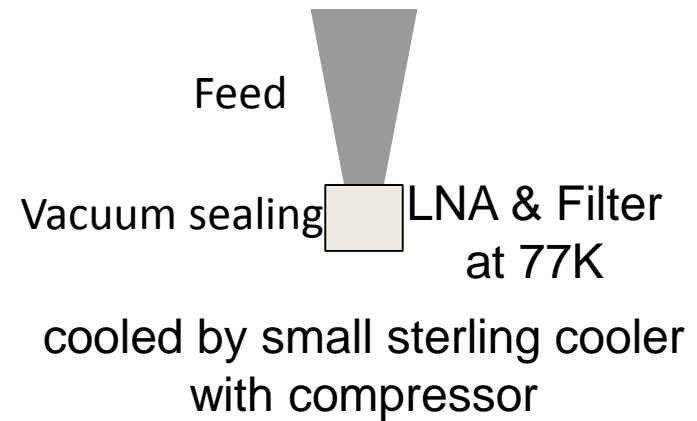
※at L-band

# Constitution of Cryo-receiver

Conventional Cryo-receiver



TOSHIBA's Cryo-receiver



- Simple constitution
- Low cost

# Compare of Receivers

Item	Conventional receiver	TOSHIBA's receiver
Power consumption	3000W	80W
Noise temperature	31K	32K
Operation temperature	20K	77K
Volume	Over 100 liters	2 liters
Weight	Over 100Kg	2Kg
Life time	About 1 year	Over 5 years
Ambient temperature	0~30 degrees	-40~55 degrees
Cooling water	necessity	unnecessary
Pipe arrangement of He	necessity	unnecessary

Energy saving, low cost,  
long life time, and high reliability

# Measurement in Usuda 64m Radio Telescope



## Actual cryo-receiver

$T_{\text{sys}}=96\text{K @}1.4\text{GHz}$

$T_{\text{sys}}=85\text{K @}1.6\text{GHz}$



-25% to -40%

## Toshiba's cryo-receiver

$T_{\text{sys}}=56\text{K @}1.4\text{GHz band}$

$T_{\text{sys}}=65\text{K @}1.6\text{GHz band}$