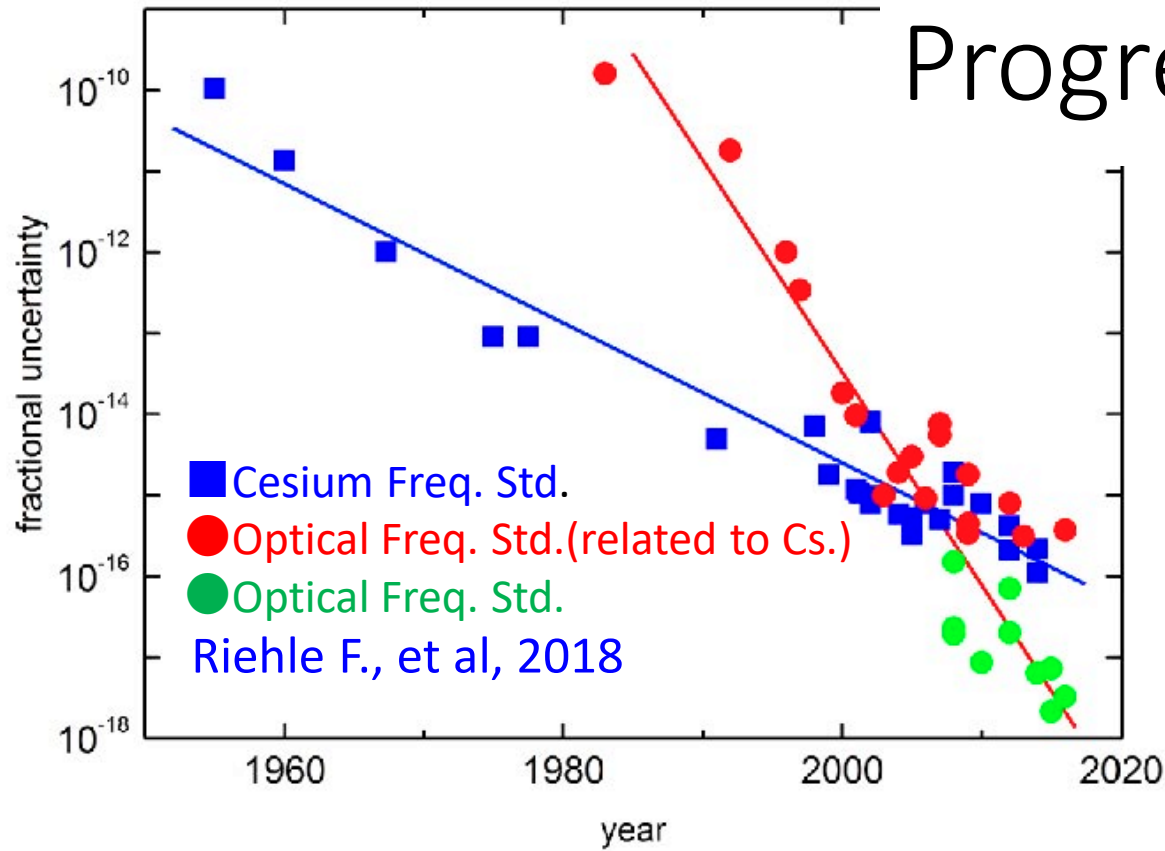


Broadband VLBI experiments with transportable stations between Italy – Japan



M.Sekido, K.Takefuji, H.Ujihara, T.Kondo, M.Tsutsumi, E.Kawai, H.Hachisu, N.Nemitz, M.Pizzocaro, C.Clivati, F.Perini, M.Negusini, G.Maccaferri, R.Ricci, M.Roma, C.Bortolotti, G.Zacchioli, J.Roda, K.Namba, J.Komuro, Y.Okamoto, R.Takahashi, R.Ichikawa, J.Leute, G.Petit, Davide Calonico, Tetsuya Ido

Progress of Optical Freq. Std.



- Uncertainty of optical freq. std reaches in order of 10^{-18} .
- Inter comparison between optical frequency standards is required.

Secondary Representation of Second

Table 2. SRS as of 2017.

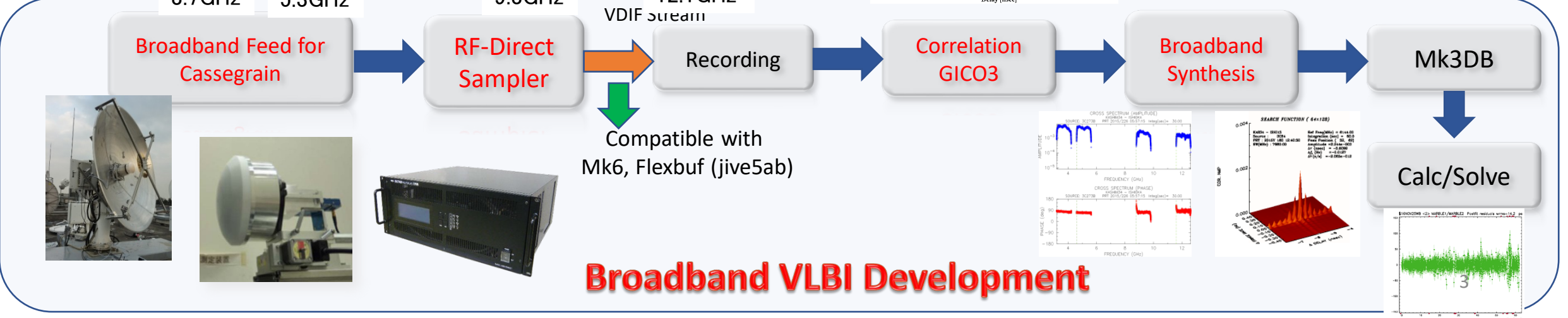
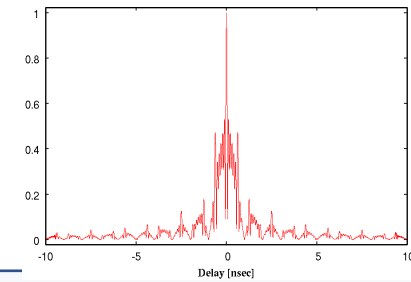
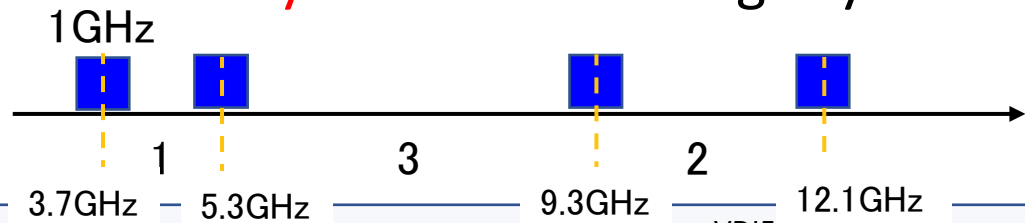
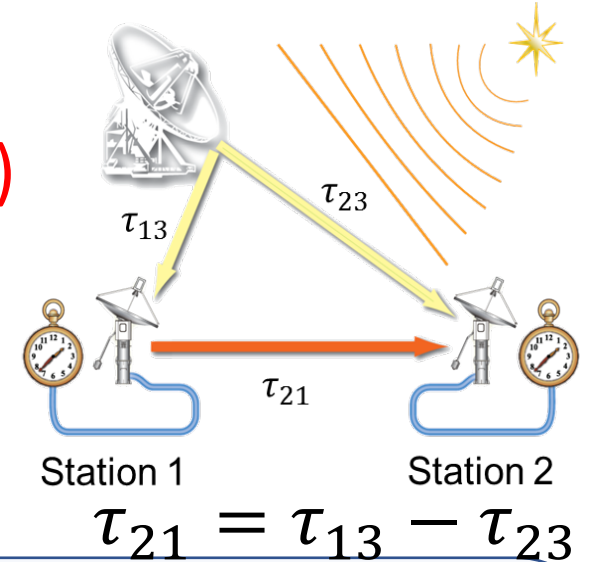
Frequency (Hz)	Fractional uncertainty	Transition
6834 682 610.904 3126	6×10^{-16}	^{87}Rb ground state hfs
429 228 004 229 873.0	4×10^{-16}	^{87}Sr neutral atom, $5s^2^1\text{S}_0-5s5p^3\text{P}_0$
444 779 044 095 486.5	1.5×10^{-15}	$^{88}\text{Sr}^+$ ion, $5s^2\text{S}_{1/2}-4d^2\text{D}_{5/2}$
518 295 836 590 863.6	5×10^{-16}	^{171}Yb neutral atom, $6s^2^1\text{S}_0-6s6p^3\text{P}_0$
642 121 496 772 645.0	6×10^{-16}	$^{171}\text{Yb}^+$ ion, $2\text{S}_{1/2}-2\text{F}_{7/2}$
688 358 979 309 308.3	6×10^{-16}	$^{171}\text{Yb}^+$ ion, $6s^2\text{S}_{1/2}-5d^2\text{D}_{3/2}$
1064 721 609 899 145.3	1.9×10^{-15}	$^{199}\text{Hg}^+$ ion, $5d^{10}6s^2\text{S}_{1/2}-5d^96s^2\text{D}_{5/2}$
1121 015 393 207 857.3	1.9×10^{-15}	$^{27}\text{Al}^+$ ion, $3s^2^1\text{S}_0-3s3p^3\text{P}_0$
1128 575 290 808 154.4	5×10^{-16}	^{199}Hg neutral atom, $6s^2^1\text{S}_0-6s6p^3\text{P}_0$

Riehle F., et al, 2018

Project Overview

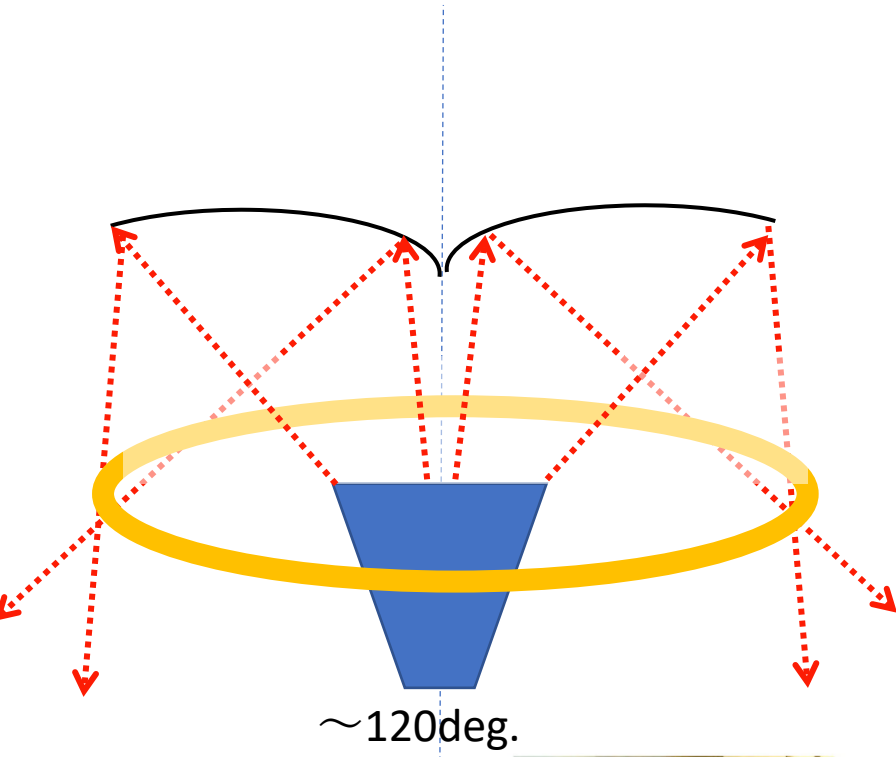
Purpose: High precision frequency comparison over intercontinental baseline toward re-definition of SI-second.

- Broad Radio Frequency : 3.2-14 GHz (Almost VGOS compatible)
- Transportable Station: Node-Hub Style VLBI
- High data-rate acquisition : 4 band (1024MHz width/band)
 - Effective Bandwidth : 3.3GHz (10 times wider than conventional)
 - Absolute delay : Free from ambiguity



Reason why NICT Developed own Broadband Feeds

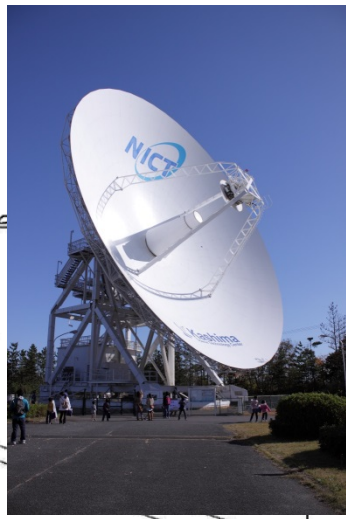
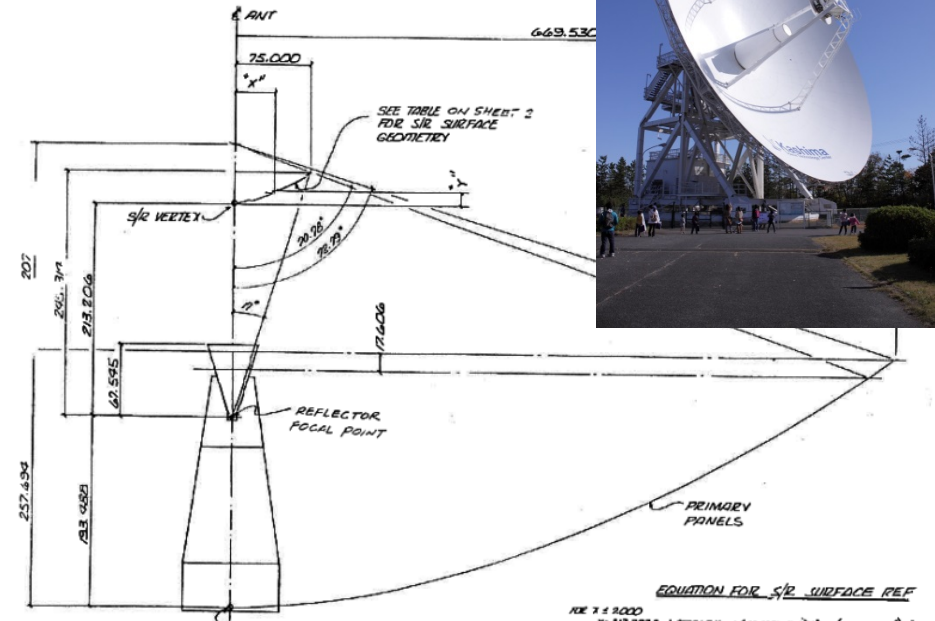
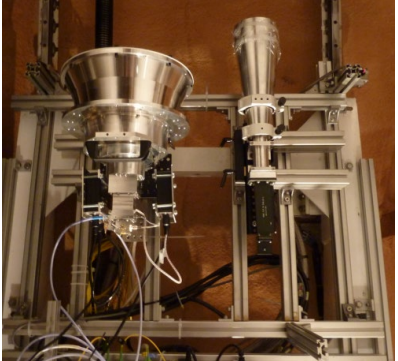
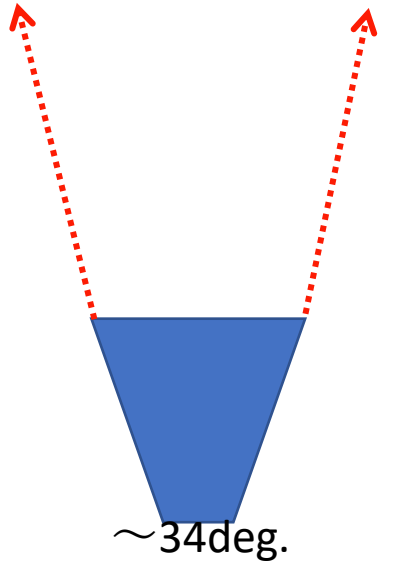
Requirement of
Broadband Frequency and
Narrow beam width



Eleven Feed



QRFH



NOTES:
1. FOR ADDITIONAL COORDINATES OF SUB-REFLECTOR CONTOUR USE EQUATION
2. SUB-REFLECTOR GEOMETRY GENERATED FROM MATRIX [A] = 1007336

EQUATION FOR s/c SURFACE REF

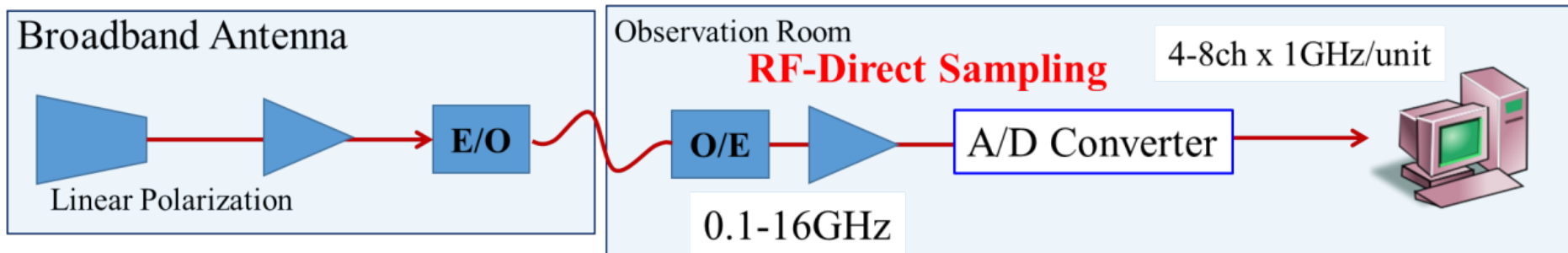
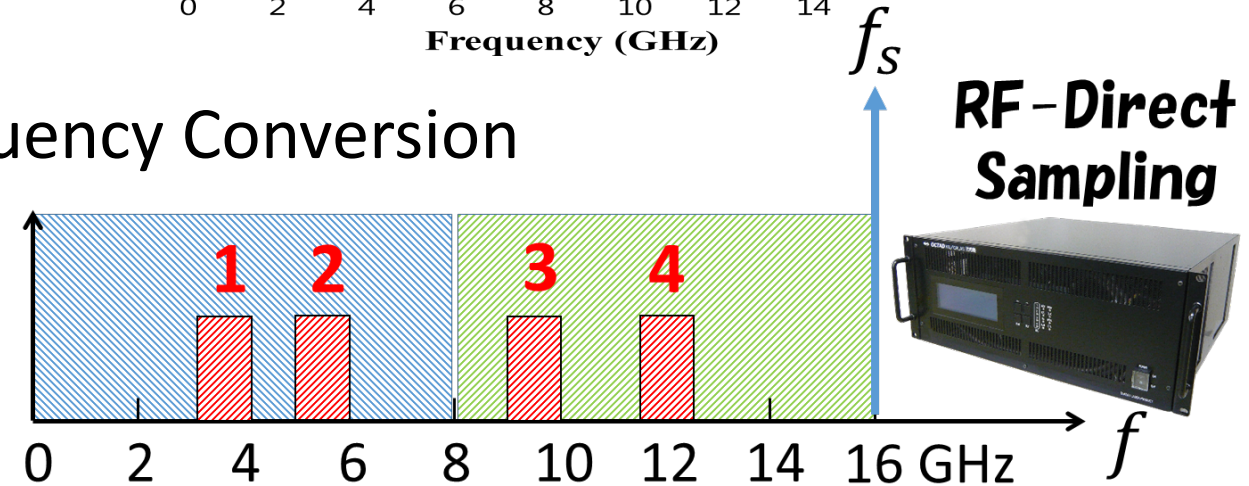
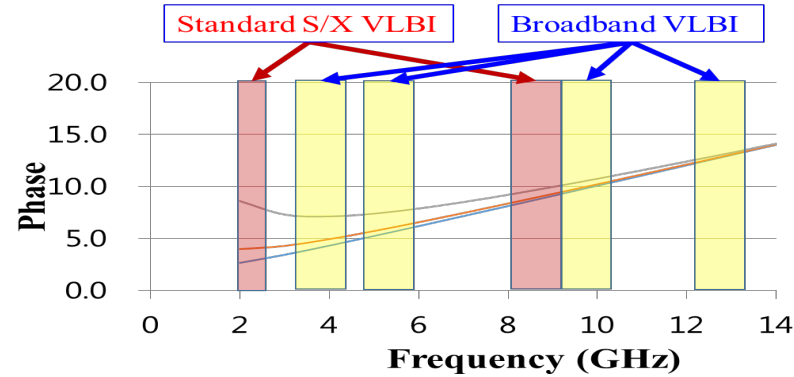
$X = 0.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) + (0.00000 X^2) - 218.2078$
$X = 15.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 30.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 45.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 60.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 75.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 90.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 105.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 120.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 135.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 150.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 165.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 180.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 195.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 210.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 225.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 240.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 255.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 270.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 285.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 300.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 315.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 330.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 345.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$
$X = 360.000$	$Y = 218.2078$	$Z = 0.00000 X^2 + (-0.00000 Y^2) - 218.2078$

Broadband Feed and RF-Direct Sampling

- Broadband VLBI, 3-14 GHz range
One order large bandwidth
→ one order fine delay precision.

• RF Direct Sampling

- Digitized without analog Frequency Conversion
- Advantage at Phase stability



A Novel features of this system

Node-Hub Style (using closure delay)

$$\tau_{21}^{NHS}(t_1) = \tau_{23}(t_1) - \tau_{13}(t_1) + \tau_{13}(t_1)\dot{t}_{21}(t_1)$$

$$\tau_{21}^{NHS} - \tau_{21}^{\text{true}} = (\tau_{31}^{\text{str}} + \tau_{23}^{\text{str}}) - \tau_{21}^{\text{str}}$$

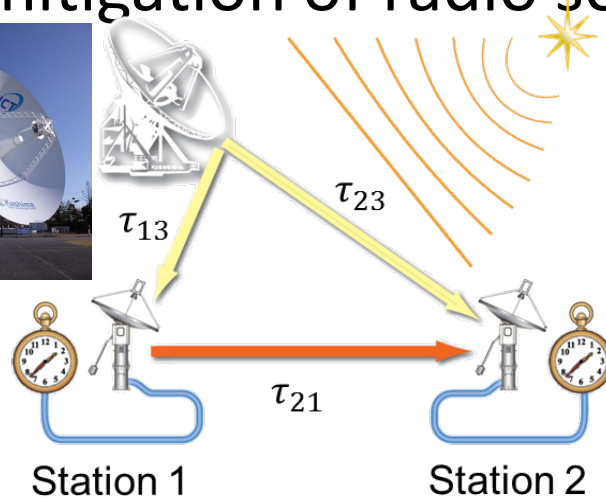
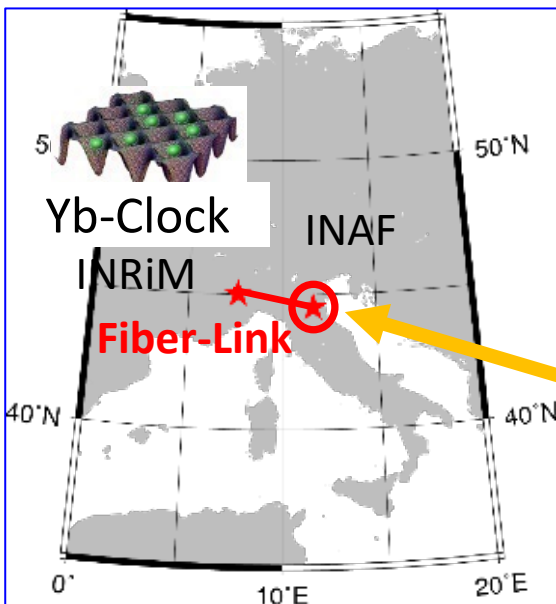
$$\text{SNR} \propto S D_1 D_2 \sqrt{\frac{\eta_1}{T_{\text{sys}1}} \cdot \frac{\eta_2}{T_{\text{sys}2}}}$$

D_n : Diameter
 S : Radio Flux
 η_n : Efficiency
 T_{sys} : System noise.

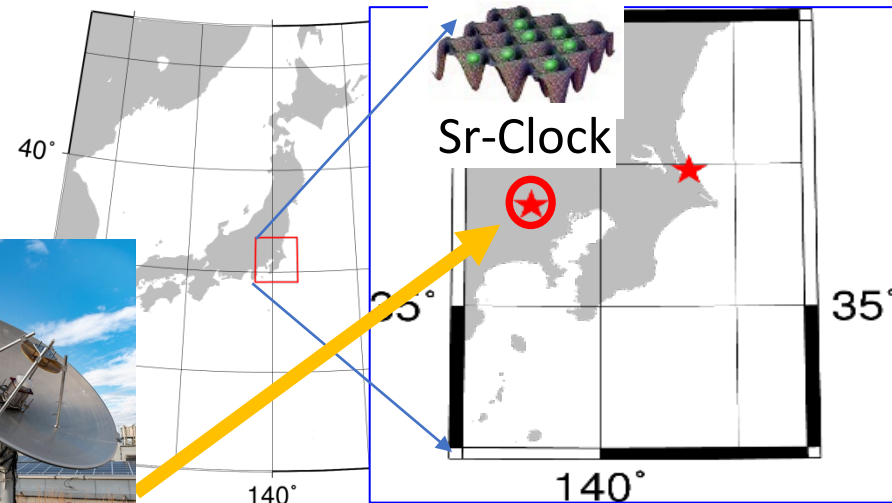
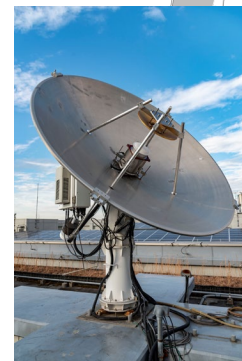
■ **Cancel effect:** Large station(Grav. Deformation, Cable delay)

■ **Easy deployment**(Small antenna): low-cost, transportable

■ **Potential advantage:** mitigation of radio source structure delay

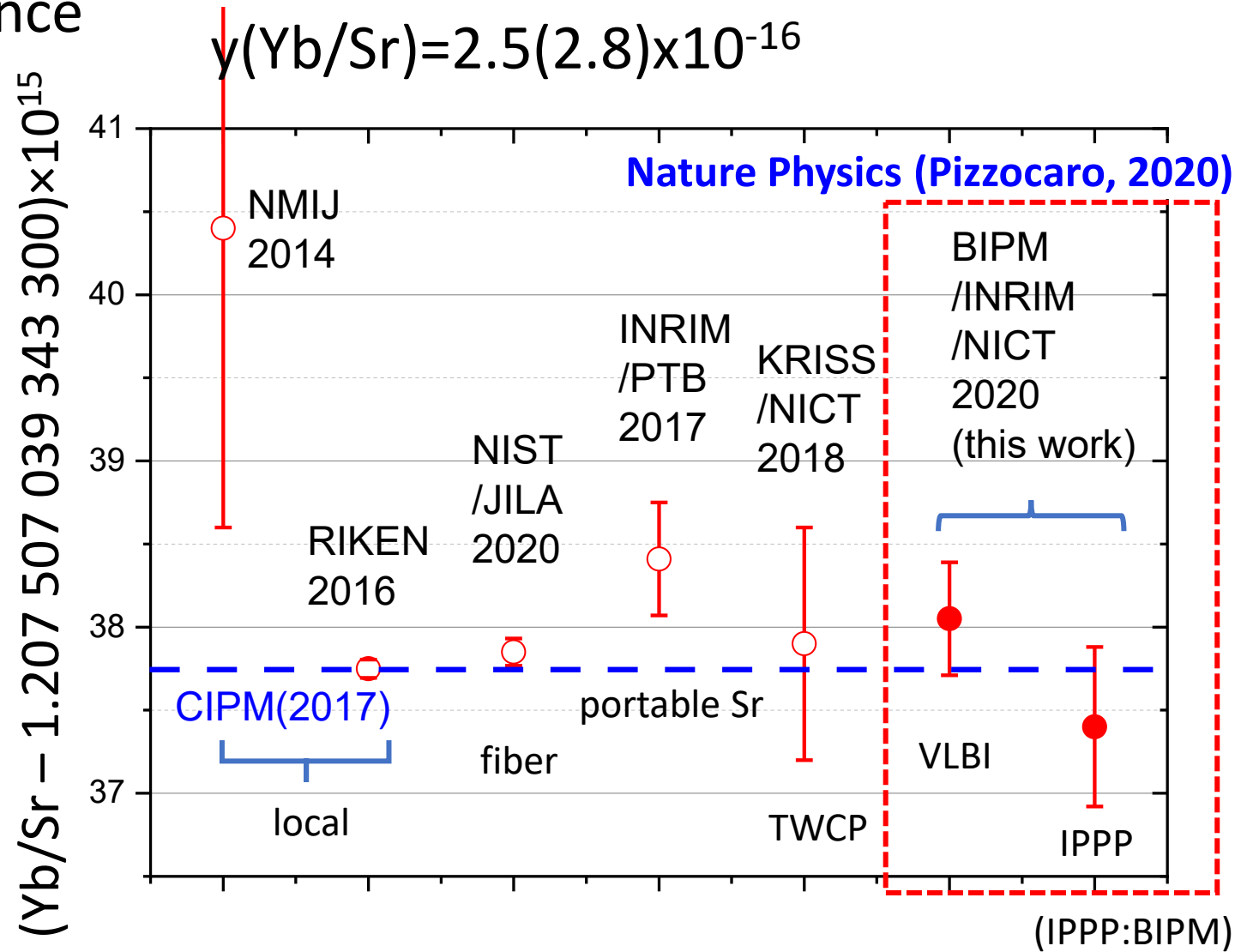
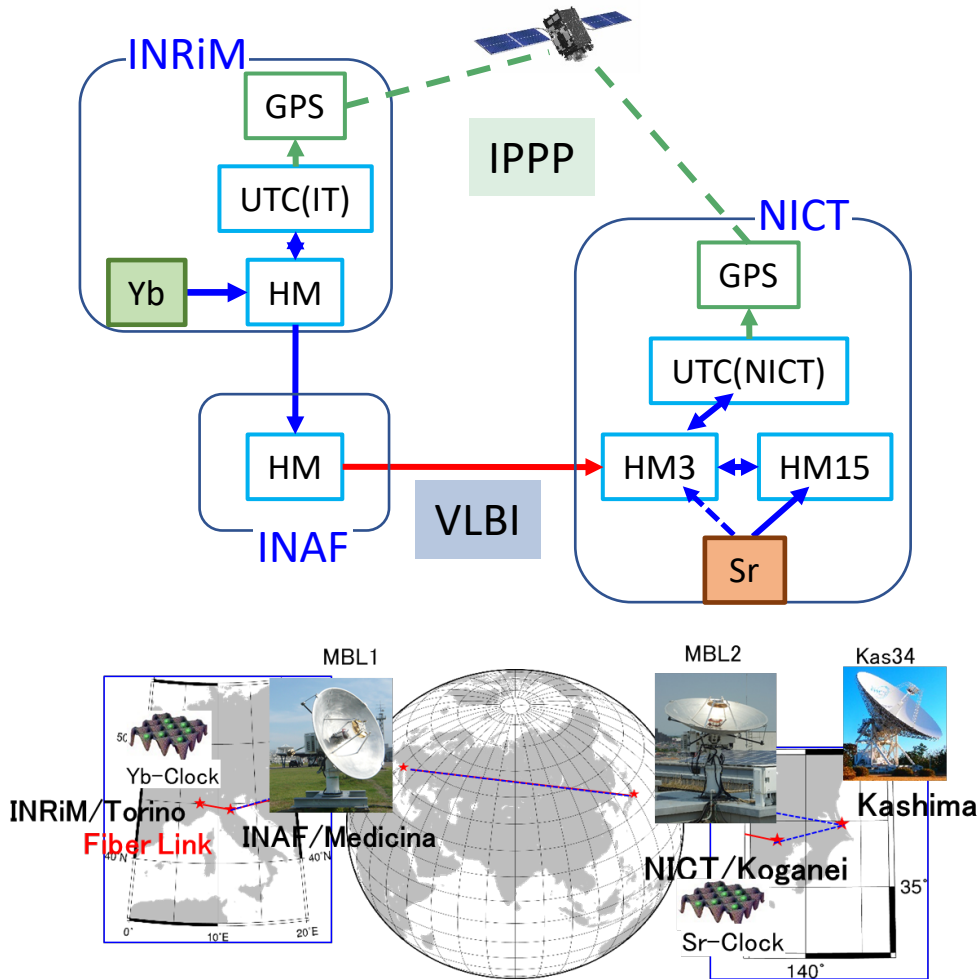


$$\tau_{21} = \tau_{13} - \tau_{23}$$



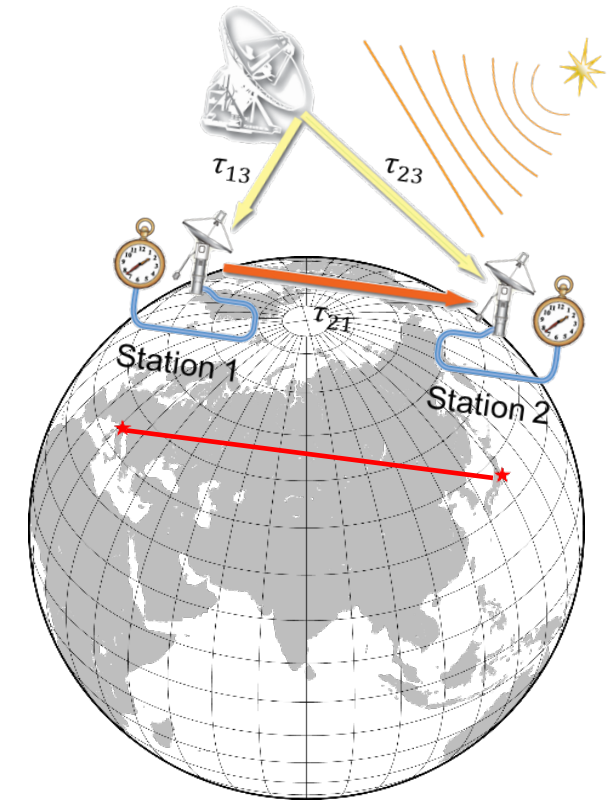
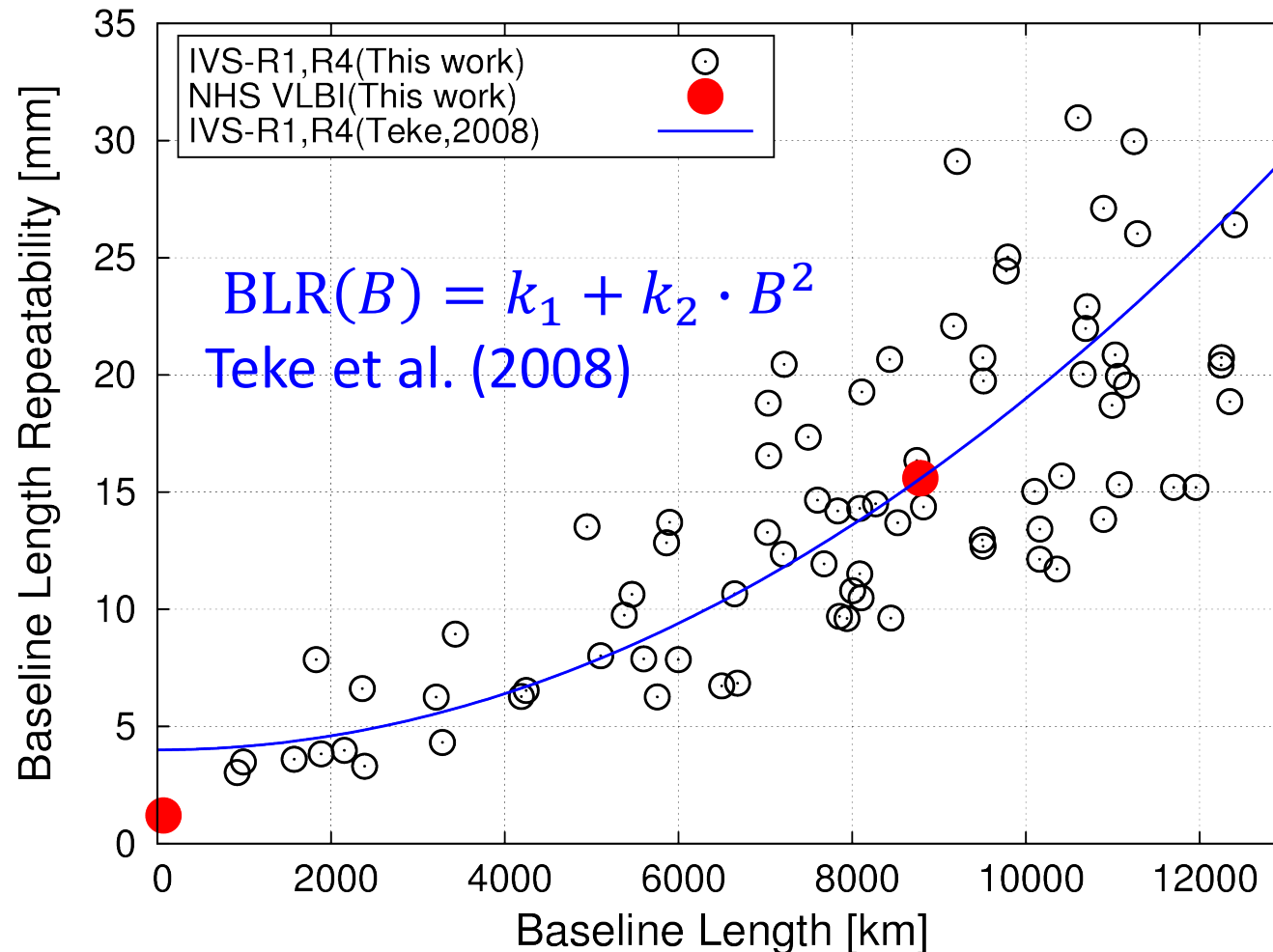
Yb/Sr Freq. Link: Comparison

Best precision for 9000 km distance



Baseline Length Repeatability (BLR)

NHS VLBI observation with 2.4m-2.4m baseline demonstrated comparable BLR performance with IVS-R1,R4 sessions.



Submitted to J. of Geodesy

Uncertainty Budget of our Broadband VLBI (Atmosphere)

$$\sigma_{\tau,obs}^2 = \sigma_{\tau,SNR}^2 + \sigma_{\tau,inst}^2 + \sigma_{\tau,atm}^2 + \sigma_{\tau,ion}^2 + \sigma_{\tau,str}^2$$

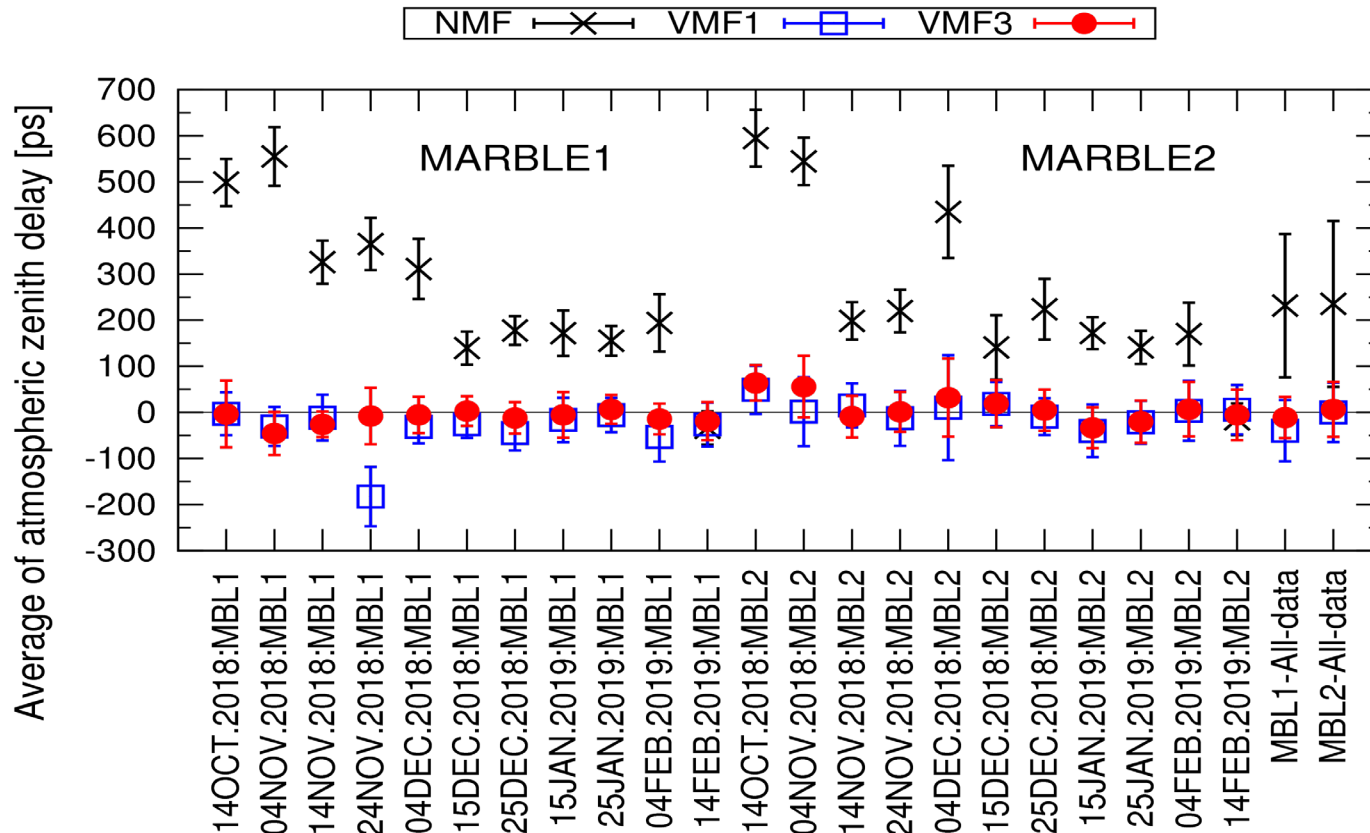
VMF3 Dry, Wet and Grad. applied as a priori.

Zero avg. of estimated zenith atm. delay residual proved accuracy of the VMF3.

The VMF3 (Vienna Mapping Function)

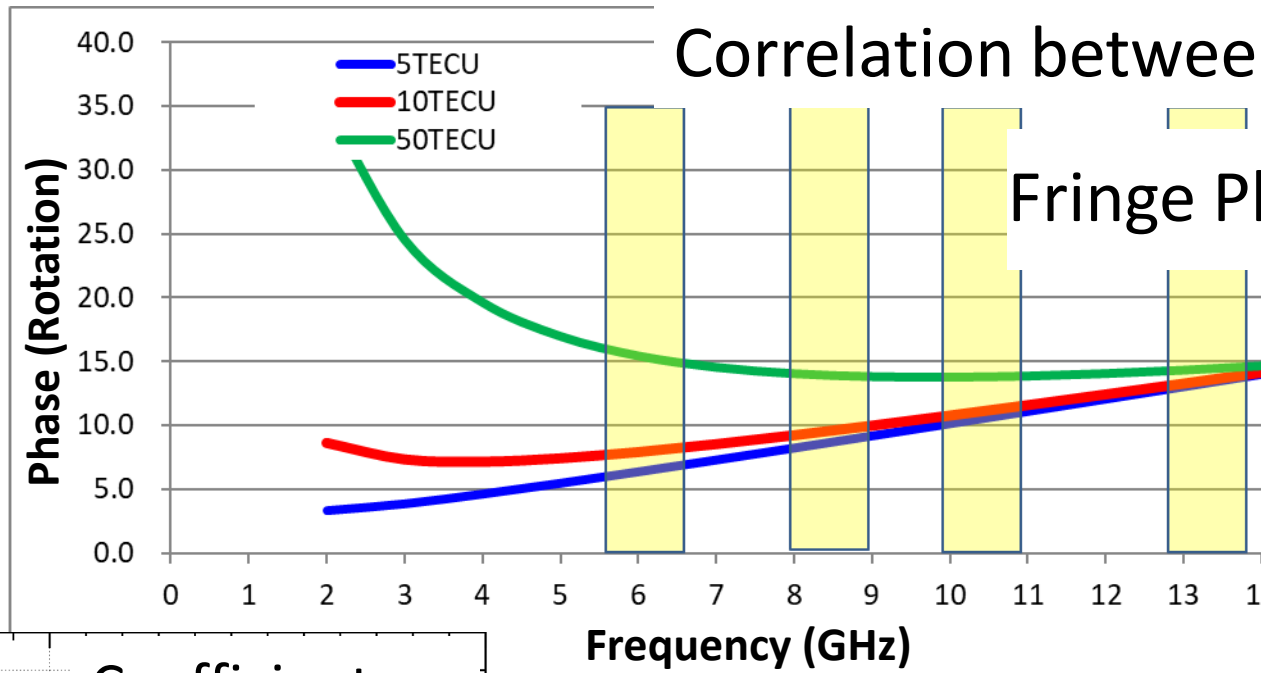
Based on ECMWF(European Centre for Medium-Range Weather Forecasts) numerical weather model

- Dry, Wet, and Gradient every 6 hours.



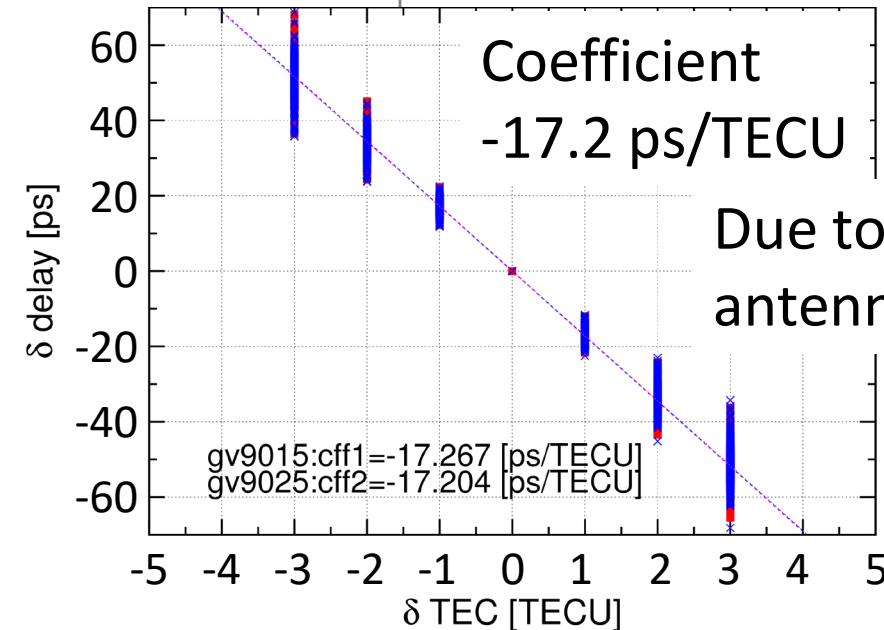
Error Source	uncertainty
Sensitivity ($\propto 1/SNR$)	6.4 ps
Instrumental	12.7 ps
Atmosphere	7.9 ps
Ionosphere	1.7~17 ps
Radio Source Structure	22-33 ps

Uncertainty Budget of Broadband VLBI (Ionosphere)



$$\text{Fringe Phase} = 2\pi\tau_g \cdot f + A \frac{\text{TEC}}{f}$$

Error Source	uncertainty
Sensitivity ($\propto 1/\text{SNR}$)	6.4 ps
Instrumental	12.7 ps
Atmosphere	7.9 ps
Ionosphere	1.7~17 ps
Radio Source Structure	22-33 ps



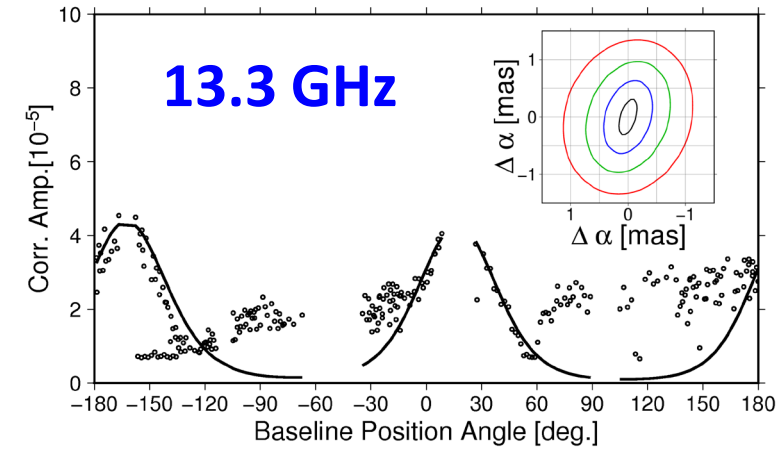
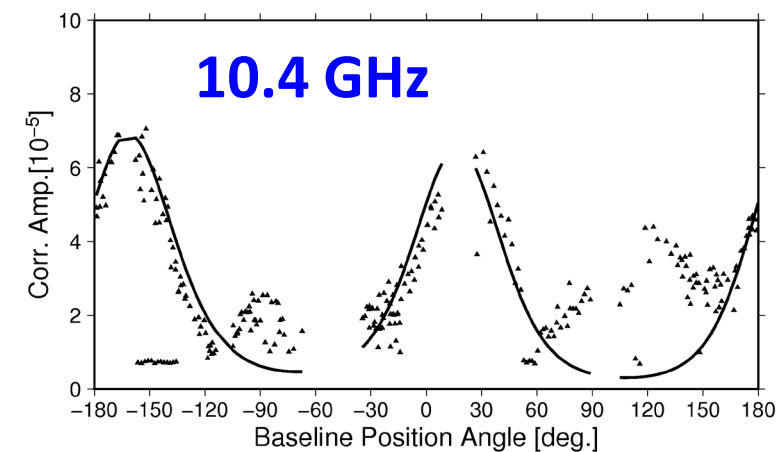
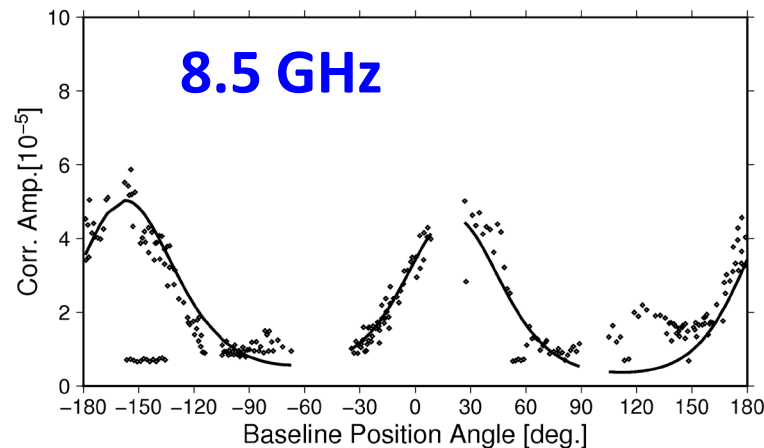
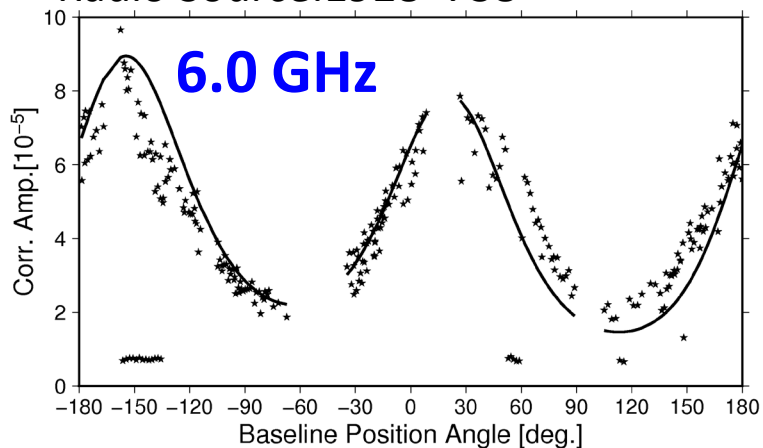
Due to limited SNR of small antenna, TEC error was 0.1-1 TECU.

Total Electron Content (TEC) is column density of electrons in the line of sight.
1 TECU = 10^{16} electrons/m²

Uncertainty Budget of our Broadband VLBI (Source Structure)

Frequency dependent source structure and barycenter shift cause **group delay error**. In addition, it also couple with ionospheric TEC.

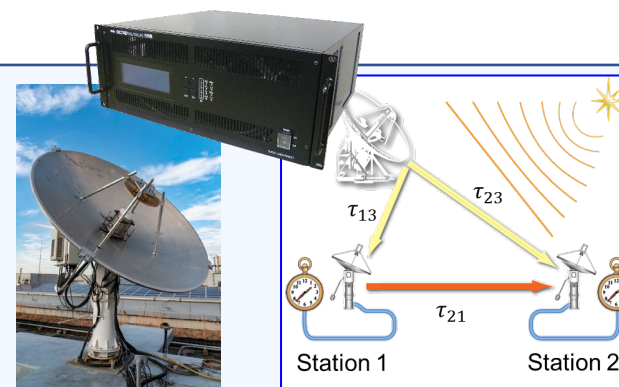
Radio Source: 1928+738



Error Source	uncertainty
Sensitivity ($\propto 1/\text{SNR}$)	6.4 ps
Instrumental	12.7 ps
Atmosphere	7.9 ps
Ionosphere	1.7~17 ps
Radio Source Structure	22-33 ps

Summary

Development: Broadband VLBI system(Feed, RF Direct-Sampling) and transportable VLBI with Node-Hub Style scheme.

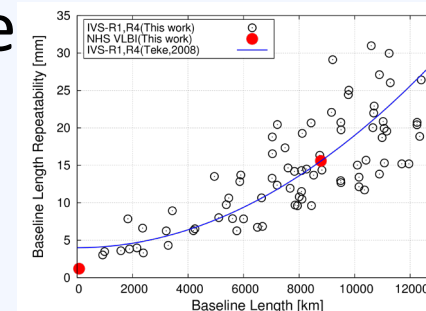


Achievement: Baseline length repeatability (BLR) was comparable with IVS-R1,R4 sessions.

Accepted at J. of Geodesy

Freq. link of Yb/Sr optical clock was made about 2.8×10^{-16} uncertainty on 9000km .

Nature physics (Pizzocaro,2020)



Acknowledgements

- We thank to colleagues of INRiM, INAF, NICT, NMIJ, for contribution to this work.
- High speed research network environment is supported by [JGN](#), [GARR](#), [GEANT](#), [Internet2](#), and [TransPAC](#).
- High speed data transfer software [JIVE5ab](#) developed by [H.Verkoeter](#) of JIVE.
- VLBI observation is supported by analysis software [Calc/Solve](#), antenna control software [Field System9](#), and scheduling software [Sked](#), all developed by [NASA/GSFC](#).